Meeting Notes

	Status Date	Item	Status / Notes	Date Assigned	Due Date	Status	Date Closed	1
▼ Myatt								
	Jul 22, 2009	• Prepare 2D analysis with details of turns of the inner PF coils						
▼ Ali Z								
	Jun 24, 2009	• Is now starting on the Axisymetric Model.	Ali presented the first set of results of the axisymmetric model					4. TF Bundle and J
▼ Chrzanowski								
	Jul 22, 2009	• Meighan working on Keystone tests of the OH conductor to verify as extruded shape	Plan to finish this test this week.Started the keystone tests, phase 1 is completed, phase 2 is next in about 2 weeks when machined conductor is available					1. Project
	Jul 22, 2009	• Need to develop method and costs to replace leaking Outer TF Leg	Jim issued a proposal to fix the outer TF water leaks	-				5. Umbrella & Oute
	Jun 24, 2009	• Use borescope to view the inside of the leak in the TF Outer leg cooling passage (during the outage).	Plan on doing this during an outage. Erik is planning on doing it early in the outage	Oct 1, 2009	TBD			5. Umbrella & Oute
▼ Denault								
	Jul 1, 2009	• Martin to look at where the pump is in it's performance curve and whether it can be modified for 600 psig head	Martin has started to look at this and will be developing a concept for the August Review	Jun 24, 2009				3. Analysis
▼ Han								
	Jul 22, 2009	• Latest runs indicate coil displacements of 4.4mm down from 17 mm. Loads in radial rods ~ 73 kips. Max stress reduced to 222 MPa. Best case scenario is Radius Rods, TF Coil to Coil Rings and no Diamond Braces.						
	Jul 1, 2009	• Working on EM diffusion model and OTF Structure	Running model still need to add more detail to determine solution					
	Jun 24, 2009	• OTF Structure: Han is adding radius rods and quantifying loads, Truss design & analysis. • Inplane, Axisym OOP, Non-axisym OOP	6/24: Hans analysis indicates the stresses in the OTF conductor do not require reinforcement. Copper stresses are around 130 MPa vs 200+ MPa Yield for 1/4 hard copper.					0. New
▼ Hatcher								
	Jun 17, 2009	• **Disruption loads have not yet been factored in. The application of a dynamic load factor less than 1.0 seems appropriate due to the impulse nature of the disruption loading.**	**Results were distributed waiting for feedback and confirmation before distributing further. Will send out results to rest of distribution.**	-	**Jun 26, 2009**	Working		**1. Project**
	Jul 8, 2009	• Need to run influence coefficients for all of the coils. Worst case current scenarios based on power supply outputs.	Distributed		7/2/09 12:00 AM			1. Project
▼ Mangra								
	Jul 22, 2009	• PF Coils are aligned by the bakeout. Expansion of the tank expands to fill the coils. It the thermal strain due to the bakeout enough to overstress the coils.						
	Jul 1, 2009	• Danny is starting to look at the PF coil support structure and determine what capacity is available. Can we support the coils as groups to minimize forces on vessel?	PF 5 alone creates forces between upper and lower ~ 400k pounds. If the forces for PF 5 are too high for the VV to bear we would change the operating scenarios to accommodate.					
▼ Menard								
	Apr 29, 2009	• The first concept of the NSTX TF Outer Leg support system has no insulating breaks. Do we need to insulate??	Menard can calculate the impact once he gets the resistance of the structure					5. Umbrella & Oute
▼ Neumeyer								
	Jul 15, 2009	• To talk to Menard about updating equlibria with realistic coil currents to be used by analysts to calculate a "realistic" set of coil loads						
▼ Perry								
	Jun 24, 2009	• Han now has the latest set of currents, displacements of the outer TF Legs are on the order of 16-17mm. Is that a concern for the machine access? What is allowable?	E. Perry believes the 16-17mm deflections can be accommodated. Need Jim C. to confirm.	Jun 10, 2009				0. New
▼ Raki								
	Jun 24, 2009	• Statement of Work for power systems PSCAD simulation tool outsourcing	This work is about 50% complete			Workiing		1. Project
▼ Sichta								
	Jul 1, 2009	• Has started to layout the cost and schedule for the I&C upgrade associated with the CSU.	First cut at the cost and schedule estimate					
▼ Sri								
	Jul 15, 2009	• SRI started to enter the Vector Potential data from Opera into the 3D model.						
	Jul 1, 2009	• Disruption Analysis of Vessel and Internals using 3d 360° model of VV.	Now have all on the required input information and now we only need to enter the data and run the model					0. New
	Jun 10, 2009	• SRI ran the OH Hoop stress model. Stresses are high at more than 160 Mpa.	May extract a few more things from the model but this work will be complete with writeup. New Run indicates stresses that are acceptable with the insulation between the OH and TF bundle.					3. Analysis
▼ Titus								
	Jul 22, 2009	• Latest run of shear loads in the TF Bundle Insulation indicate stresses of ~ 20MPa vs 40MPa allowable						
	Jul 1, 2009	• Global Model, Running, not merged well, corrections being made.	HM -Passive Plates & Upper and Lower VV, Han - TF Loop Geometry, Sri - Mid Plane Ports, HM/Sri - VV Support Structure					0. New
		• Document OOP and IP loading						3. Analysis
▼ Willard								
	Jul 15, 2009	• Tom Willard is working on the local mechanical details of the bolted connection, flag. Using .3 Tesla field from Hatcher.	Thicker laminations are an improvement but the fatique life is still inadequate. Making the loop shorter should help the fatique life. Will investigate the practicality of that change with the designer.	Jun 10, 2009				3. Analysis
▼ Woolley								
	Jun 10, 2009	• A coil protection system needs to be incorporated into the project plans to ensure that the envelope is suitably constrained.	Reassigned to Woolley	Jun 10, 2009	Jun 30, 2009	Working		2. Design Requirem