

Meeting Notes

	Item	Respon.	Date Assigned	Due Date	Status Date	Status / Notes
▼ 0. New						
	New Jun 10th					
	<ul style="list-style-type: none"> New PF1A, B & C dimensions are being laid out by Lew Morris for review by Neumeyer, Menard, et al. 		Jun 10, 2009		Jun 10, 2009	
	<ul style="list-style-type: none"> PF 3 +/- 480 may be driving the stresses in the ring. Need to check the stresses in the TF Coil. Han will add tangential tension spokes to restrict the rotation of the ring assembly. Dudek to set up tour of the machine with Titus and Han to look for best locations for restraints (during maint weeks) 	Zhang	Jun 10, 2009		Jun 10, 2009	
	<ul style="list-style-type: none"> Han now has the latest set of currents, displacements are on the order of 16-17mm. Is that a concern for the machine access? What is allowable? 	Perry	Jun 10, 2009		Jun 10, 2009	
	<ul style="list-style-type: none"> Reviewed the list of analysis and clarified the requirements for the CDR. By Monday should have a new list for Strykowski to incorporate in the CDR Plan. 	--			Jun 10, 2009	
	<ul style="list-style-type: none"> Tom Willard is working on the local mechanical details of the bolted connection, flag. Using .3 Tesla field from Hatcher. 	Willard	Jun 10, 2009		Jun 10, 2009	
▼ 1. Project						
	<ul style="list-style-type: none"> Statement of Work for power systems PSCAD simulation tool outsourcing 	Ramakrishnan			Jun 10, 2009	Still in the works
	<ul style="list-style-type: none"> Meighan working on Keystone tests of the OH conductor to verify as extruded shape 	Chrzanowski			May 27, 2009	Working setting up for tests. Ordering material.
	<ul style="list-style-type: none"> Disruption loads have not yet been factored in. The application of a dynamic load factor less than 1.0 seems appropriate due to the impulse nature of the disruption loading. 	Hatcher	-	Apr 2, 2009	Jun 10, 2009	Working on the results should transmit results today
▼ 2. Design Requirements						
	<ul style="list-style-type: none"> A more limited OH and PF operating envelope needs to be developed for the design basis assumption 	Neumeyer	Mar 1, 2009	Apr 15, 2009	May 6, 2009	Made a lot of progress need one more meeting.
	<ul style="list-style-type: none"> A coil protection system needs to be incorporated into the project plans to ensure that the envelope is suitably constrained. 	Woolley	Jun 10, 2009	Jun 30, 2009	Jun 10, 2009	Reassigned to Woolley
▼ 3. Analysis						
	<ul style="list-style-type: none"> HAN has developed a model of the TF Turn with cooling 	Han			Apr 29, 2009	Need to have Neumeyer verify the currents that HAN is using in the model
	<ul style="list-style-type: none"> Document OOP and IP loading 	Titus				
	<ul style="list-style-type: none"> Ali Z working on the OH Cooling analysis. Expect to be done by end of June 	Ali Z	Jun 30, 2009		Jun 10, 2009	Initial results show longer cooling times with .188 dia and 400 psig. Will look at effect of taking into account the turn to turn heat transfer.
	<ul style="list-style-type: none"> Martin to look at where the pump is in it's performance curve and whether it can be modified for 600 psig head 	Denault	Jun 24, 2009		Jun 10, 2009	
	<ul style="list-style-type: none"> HAN needs to run confirmation of hoop tension by adding in the vertical field from Hatcher once he gets the coil dimensions from Bruce Paul (Jim C. to take action) 	Chrzanowski			May 13, 2009	Hatcher just iterating data with designer to develop the model. Han to run stress pass to compare with Titus's results in same area. (Looking for maximum vertical field)
	<ul style="list-style-type: none"> SRI ran the OH Hoop stress model. Stresses are high at more than 160 Mpa. 	Sri			Jun 10, 2009	May extract a few more things from the model but this work will be complete with writeup. New Run indicates stresses that are acceptable with the insulation between the OH and TF bundle.
	<ul style="list-style-type: none"> Han presented the latest outer TF leg support analysis. Looks like cross bracing is only needed in four locations. 	Zhang	-	Mar 25, 2009	May 13, 2009	For now we will stay with the existing "diamond brace" design. Mangra looking at space needs and has some ideas on how to minimize space impact of the structural design. (This analysis still needs to be checked) The latest analysis shows that with some simple "ring" reinforcement at the TB level and diagonal bracing at four bays we reduce the outer TF connection reactions to manageable levels. Han, just need loads in ring and cross brace members. Dudek provided cross section information of stainless steel members for next step analysis
	<ul style="list-style-type: none"> SRI has started on the bolting analysis. 	SRI			Jun 10, 2009	Need to coordinate with Willard work
▼ 5. Umbrella & Outer TF Leg						
	<ul style="list-style-type: none"> The first concept of the NSTX TF Outer Leg support system has no insulating breaks. Do we need to insulate?? 	--			Apr 29, 2009	Menard can calculate the impact once he gets the resistance of the structure
	<ul style="list-style-type: none"> Need to develop method to seal existing leaks in Outer TF Leg cooling passages 	Chrzanowski	-		May 27, 2009	Requisition is out
	<ul style="list-style-type: none"> Use borescope to view the inside of the leak in the TF Outer leg cooling passage (during the outage). 	Chrzanowski	Oct 1, 2009	TBD	Apr 8, 2009	Plan on doing this during an outage.
▼ 6. VV Structure						
	<ul style="list-style-type: none"> Enhance the VV midplane strength by welding a band of material around the inner surface of the midplane, where interferences are relatively minor. 	Heitzenroeder	-	Ongoing	Mar 25, 2009	Need to look at the strength of the vv with ports (Global Model) Need to rerun with 360 degree model to refine the analysis.