

OH Coil Pre Load System

TF hot OH cold

Calculations for the least critical system scenario.

From Pre Load of 17.87 mm

8.4 mm of compression are released due to the
TF coil thermal expansion = 8.4 mm

Therefore, the total compression on the
Spring stack is = 9.47 mm

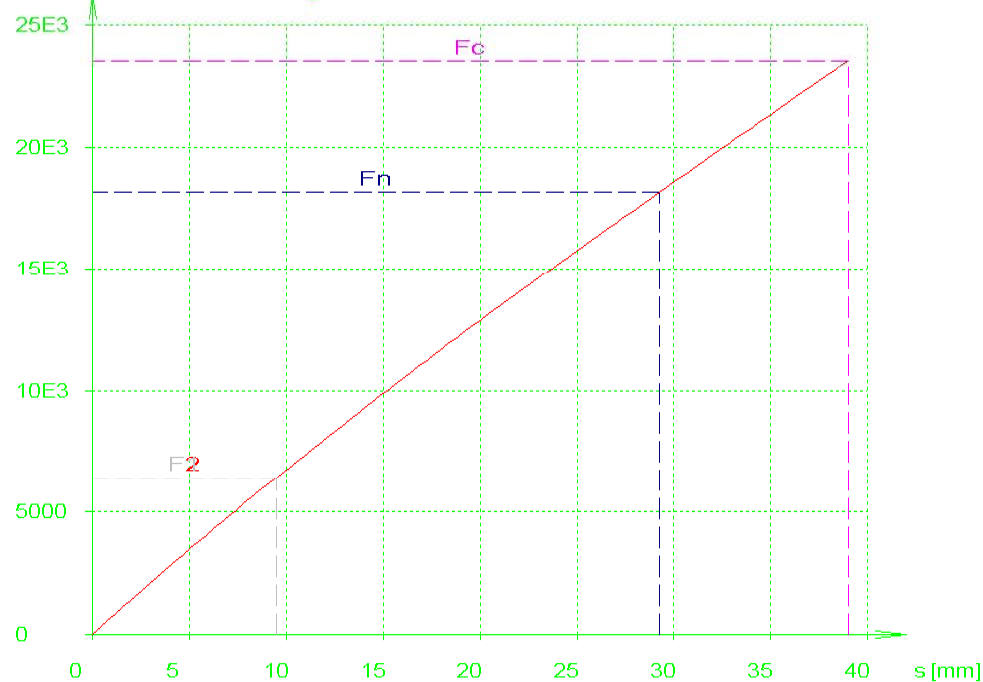
For a single spring $s = .364$ mm

For the stack = $.3642 \times 26 = 9.47$ mm

Maximum obtained force on the OH coil

With 14 stacks = $6,407. \times 14 = 89,698$ N
(20,157. lbs.)

Force Path Diagram



$D_i = 30.5 \text{ mm}$
 $D_e = 60 \text{ mm}$
 $t = 3.5 \text{ mm}$
 $L_0 = 5 \text{ mm}$

$n_f = 1$
 $n_p = 26$
 $L_c = 91 \text{ mm}$
 $L_0 = 130 \text{ mm}$

Stainless Steel Required

$E = 206000 \text{ MPa}$
 $\mu = 0.3$
 $\rho = 7.85 \text{ kg/dm}^3$
 $\sigma_{perm} = 1230 \text{ MPa}$
 (DIN 2092)

messages

- none -

Pre Load was = 17.87 mm

-TF hot = 8.4 mm

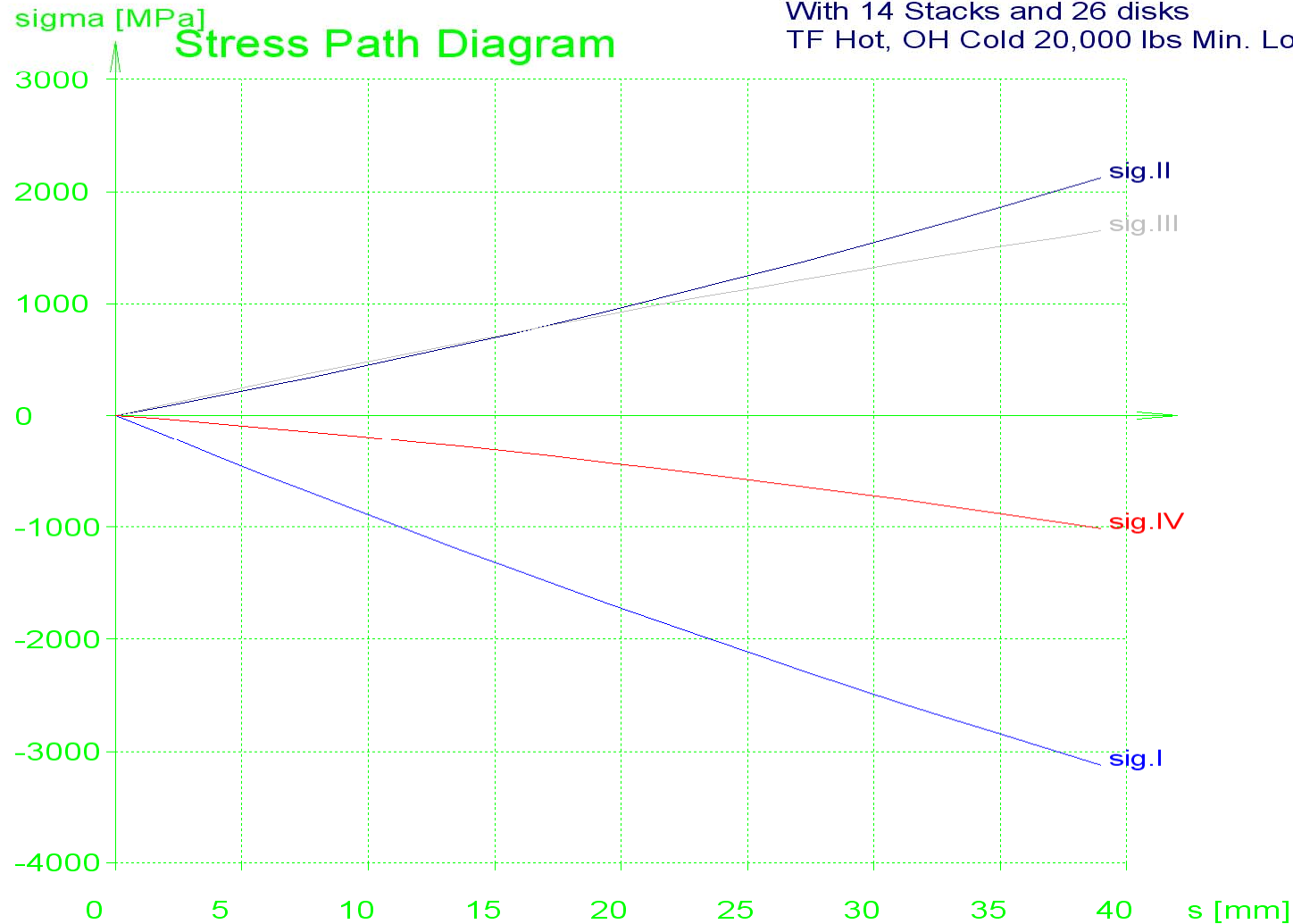
Total compression = 9.47 mm

Total Force/Stack = 6,411. N
(1,441. lbs.)

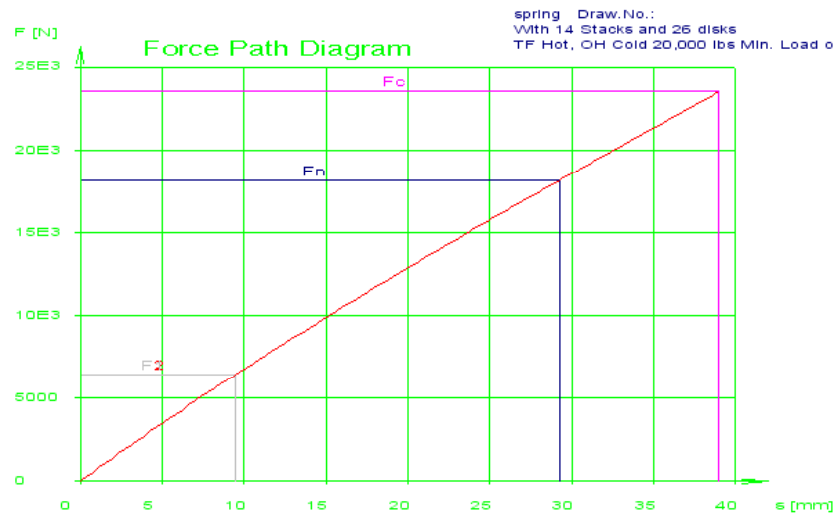
Constant Force on OH coil
(1,441 x 14 = 20,169. lbs)

	0	1	2	n	c	
s	0.00	9.47	9.47	29.25	39.00	mm
L	130.00	120.53	120.53	100.75	91.00	mm
F	0	6411	6411	18153	23528	N
R	18566	16723	16723	14515	14245	N/mm
sigma I	0	-850	-850	-2434	-3121	MPa
sigma III	0	459	459	1297	1650	MPa
si	0.00	0.36	0.36	1.13	1.50	mm
Li	5.00	4.64	4.64	5.00	0.00	mm
Fi	0	6411	6411	18153	23528	N

spring Draw.No.:
With 14 Stacks and 26 disks
TF Hot, OH Cold 20,000 lbs Min. Load on OH



$D_i = 30.5$ H12
 $D_e = 60$ H12
 $t = 3.5$
 $L_0 = 5$
 $\sigma_{\text{mean}} = -850$ MPa
 $\sigma_{\text{maxI}} = 424$ MPa
 $\sigma_{\text{maxII}} = 459$ MPa
 $\sigma_{\text{maxIV}} = -188$ MPa
 $n_f = 1$
 $n_p = 26$
 $F_1 = 6411$ N
 $F_2 = 6411$ N
 $F_n = 18153$ N
 $F_c = 23528$ N
 $sh = 0$
 $s_1 = 9.47$
 $s_2 = 9.47$
 $s_n = 29.25$
 $sc = 39$
 $L_0 = 130$
 $L_1 = 120.5$
 $L_2 = 120.5$
 $L_n = 100.8$
 $L_c = 91$
 $R_1 = 16723$ N/mm
 $R_2 = 16723$ N/mm



$D_i = 30.5 \text{ H12}$
 $D_o = 60 \text{ H12}$
 $t = 3.5$
 $L_0 = 5$
 $\sigma_{max} = 850 \text{ MPa}$
 $\sigma_{min} = 424 \text{ MPa}$
 $\sigma_{avg} = 459 \text{ MPa}$
 $\sigma_{V} = 188 \text{ MPa}$
 $n_f = 1$
 $n_p = 26$
 $F_1 = 6411 \text{ N}$
 $F_2 = 6411 \text{ N}$
 $F_n = 18153 \text{ N}$
 $F_c = 23528 \text{ N}$
 $sh = 0$
 $s_1 = 9.47$
 $s_2 = 9.47$
 $sn = 29.25$
 $sc = 39$
 $L_0 = 130$
 $L_1 = 120.6$
 $L_2 = 120.5$
 $L_n = 100.8$
 $L_c = 91$
 $R_1 = 16723 \text{ N/mm}$
 $R_2 = 16723 \text{ N/mm}$

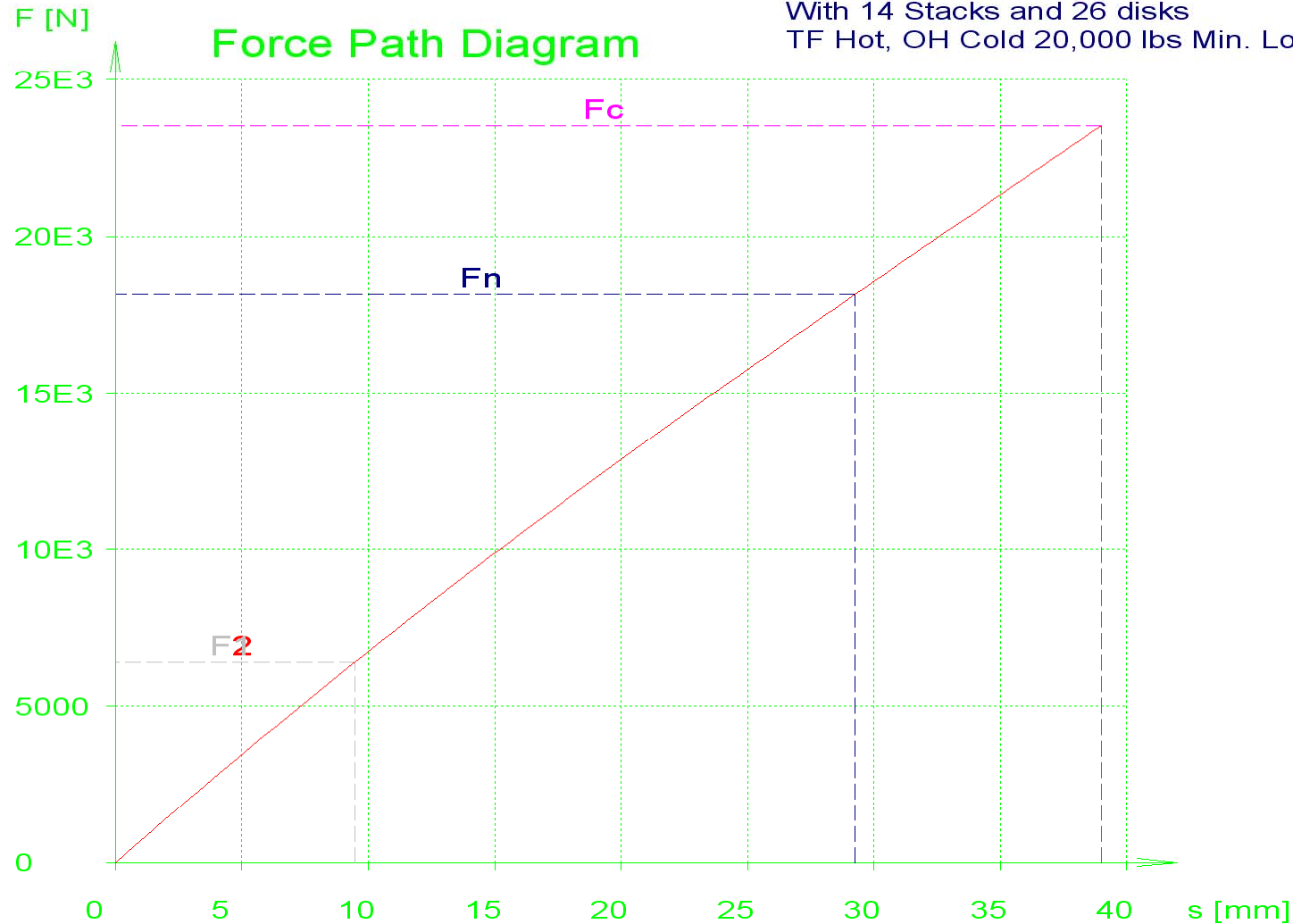
spring Draw.No.:
With 14 Stacks and 26 disks
TF Hot, OH Cold 20,000 lbs Min. Load on OH

SINGLE DISK SPRING			
inside diameter	D_i	mm	30.5 H12
outside diameter	D_o	mm	60 H12
thickness	t	mm	3.5
length	L_0	mm	5
weight	m	g	57.61
usable spring travel $sn=0.75 \cdot h_0$	sin	mm	1.125
max. spring travel $h_0=sc$	sic	mm	1.5
spring force with $sn=0.75 \cdot sc$	F_{in}	N	18153
No. of springs per package	n_f		1
No. of spring packages	n_p		26

Length mm	Sp.travel mm	Load N	Sigma MPa
$L_0 = 130.00$			
$L_1 = 120.53$	$s_1 = 9.47$	$F_1 = 6411.21$	$\sigma_{max1} = 459$
	$sh = 0.00$	$F_h = 0.00$	$\sigma_{mah} = 0$
$L_2 = 120.53$	$s_2 = 9.47$	$F_2 = 6411.21$	$\sigma_{max2} = 459$
$L_n = 100.75$	$sn = 29.25$	$F_n = 18152.58$	$\sigma_{man} = 1297$
$L_c = 91.00$	$sc = 39.00$	$F_c = 23528.21$	$\sigma_{mac} = 1650$

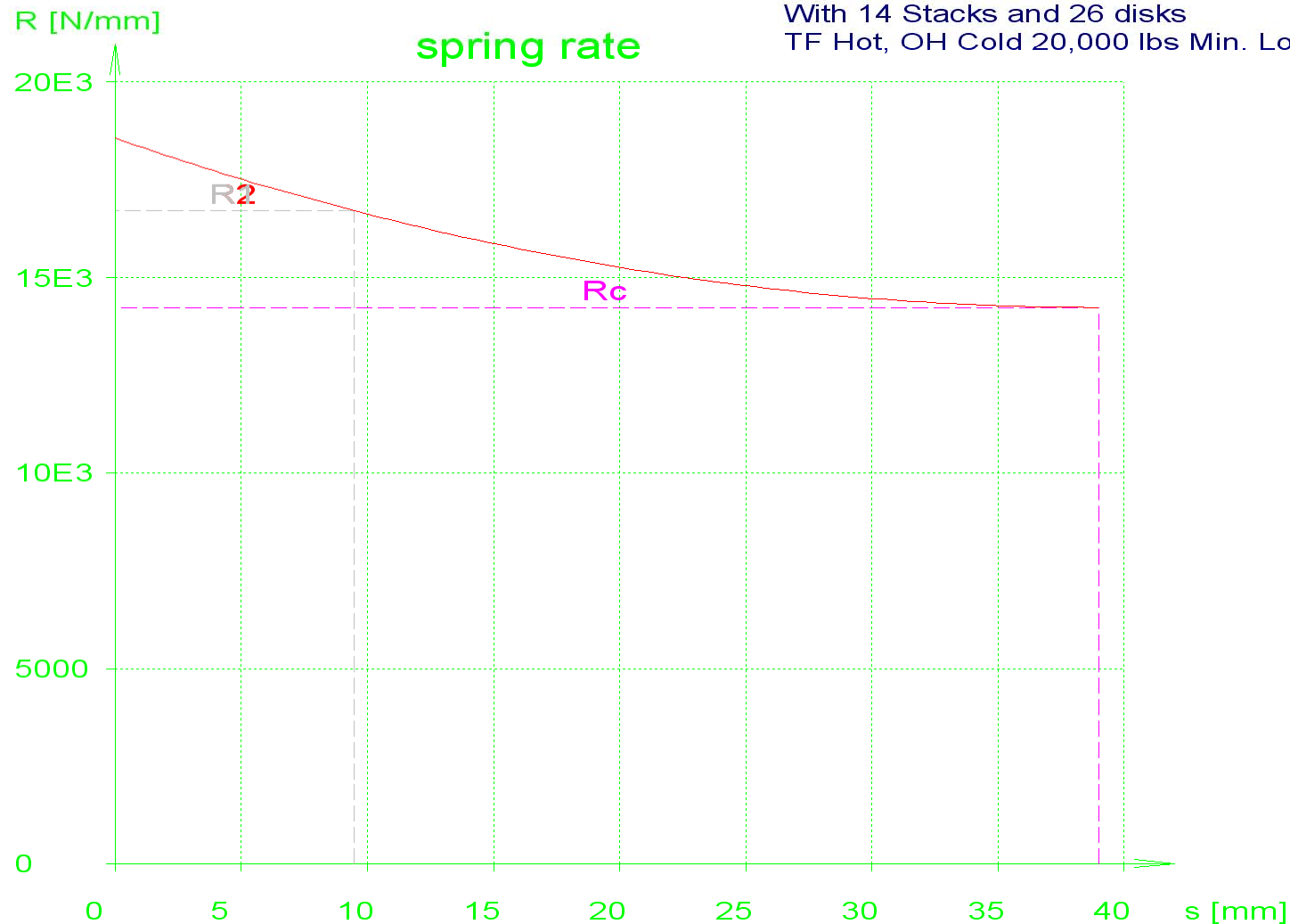
				Date	Name	Disk Spring		
				Compl.	08/25/2010			P. Rogoff
				Check				
				Stand.				
Cond.	Modification	Date	Name	Princeton Plasma Physics Lab				

spring Draw.No.:
With 14 Stacks and 26 disks
TF Hot, OH Cold 20,000 lbs Min. Load on OH



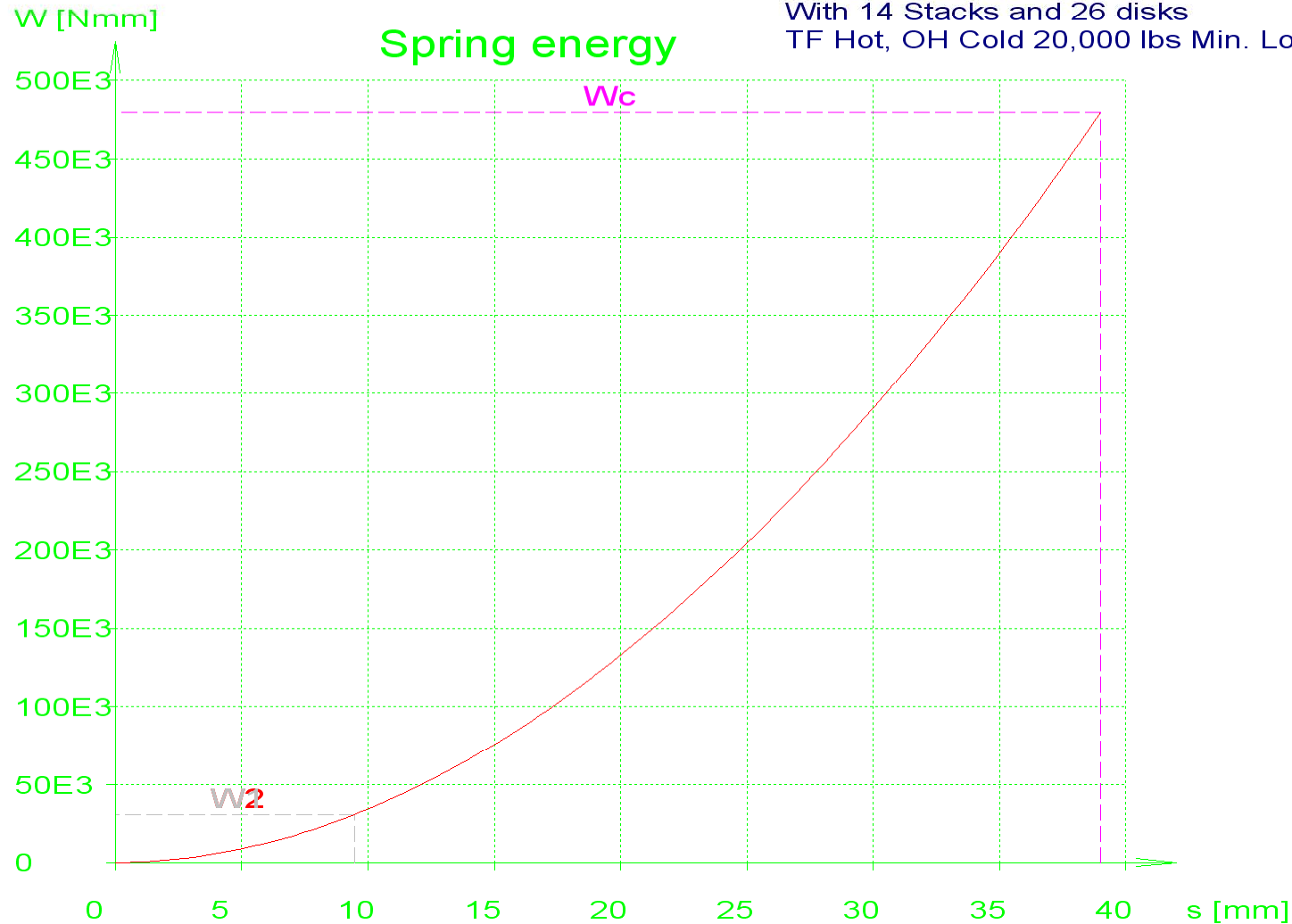
$D_i = 30.5$ H12
 $D_e = 60$ H12
 $t = 3.5$
 $L_0 = 5$
 $\text{signal} = -850$ MPa
 $\text{sigmall} = 424$ MPa
 $\text{sigmalll} = 459$ MPa
 $\text{signalV} = -188$ MPa
 $n_f = 1$
 $n_p = 26$
 $F_1 = 6411$ N
 $F_2 = 6411$ N
 $F_n = 18153$ N
 $F_c = 23528$ N
 $sh = 0$
 $s_1 = 9.47$
 $s_2 = 9.47$
 $s_n = 29.25$
 $s_c = 39$
 $L_0 = 130$
 $L_1 = 120.5$
 $L_2 = 120.5$
 $L_n = 100.8$
 $L_c = 91$
 $R_1 = 16723$ N/mm
 $R_2 = 16723$ N/mm

spring Draw.No.:
With 14 Stacks and 26 disks
TF Hot, OH Cold 20,000 lbs Min. Load on OH



Di = 30.5 H12
De = 60 H12
t = 3.5
L0 = 5
signal = -850 MPa
sigmall = 424 MPa
sigmalll = 459 MPa
signalV = -188 MPa
nf = 1
np = 26
F1 = 6411 N
F2 = 6411 N
Fn = 18153 N
Fc = 23528 N
sh = 0
s1 = 9.47
s2 = 9.47
sn = 29.25
sc = 39
L0 = 130
L1 = 120.5
L2 = 120.5
Ln = 100.8
Lc = 91
R1 = 16723 N/mm
R2 = 16723 N/mm

spring Draw.No.:
With 14 Stacks and 26 disks
TF Hot, OH Cold 20,000 lbs Min. Load on OH



$D_i = 30.5$ H12
 $D_e = 60$ H12
 $t = 3.5$
 $L_0 = 5$
 $\text{signal} = -850$ MPa
 $\text{sigall} = 424$ MPa
 $\text{sigallI} = 459$ MPa
 $\text{sigalV} = -188$ MPa
 $n_f = 1$
 $n_p = 26$
 $F_1 = 6411$ N
 $F_2 = 6411$ N
 $F_n = 18153$ N
 $F_c = 23528$ N
 $sh = 0$
 $s_1 = 9.47$
 $s_2 = 9.47$
 $sn = 29.25$
 $sc = 39$
 $L_0 = 130$
 $L_1 = 120.5$
 $L_2 = 120.5$
 $L_n = 100.8$
 $L_c = 91$
 $R_1 = 16723$ N/mm
 $R_2 = 16723$ N/mm

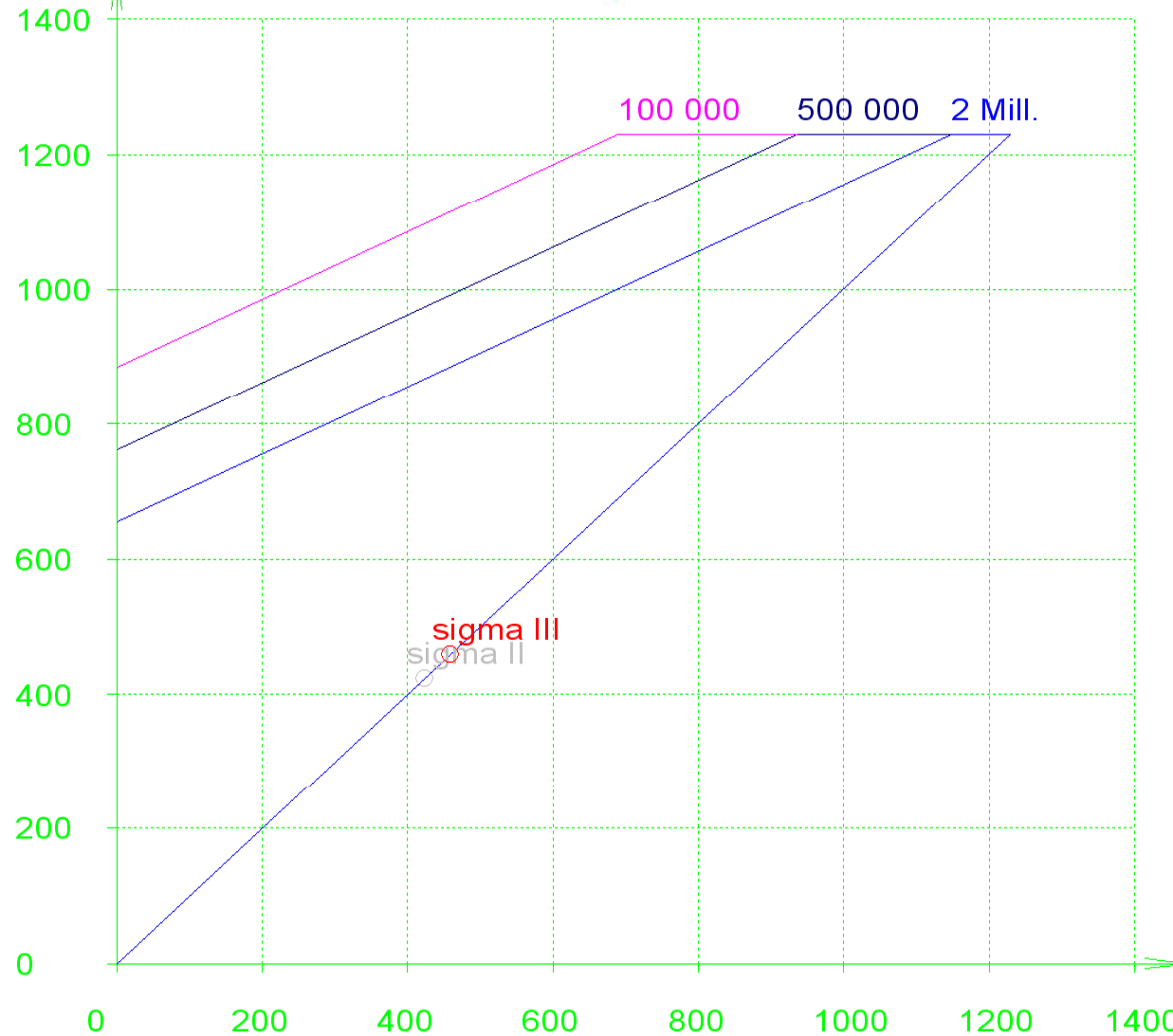
spring Draw.No.:

With 14 Stacks and 26 disks

TF Hot, OH Cold 20,000 lbs Min. Load on OH

sig.o [MPa]

Goodman diagram



Di = 30.5 H12

De = 60 H12

t = 3.5

L0 = 5

signal = -850 MPa

sigall = 424 MPa

sigallI = 459 MPa

sigalV = -188 MPa

nf = 1

np = 26

F1 = 6411 N

F2 = 6411 N

Fn = 18153 N

Fc = 23528 N

sh = 0

s1 = 9.47

s2 = 9.47

sn = 29.25

sc = 39

L0 = 130

L1 = 120.5

L2 = 120.5

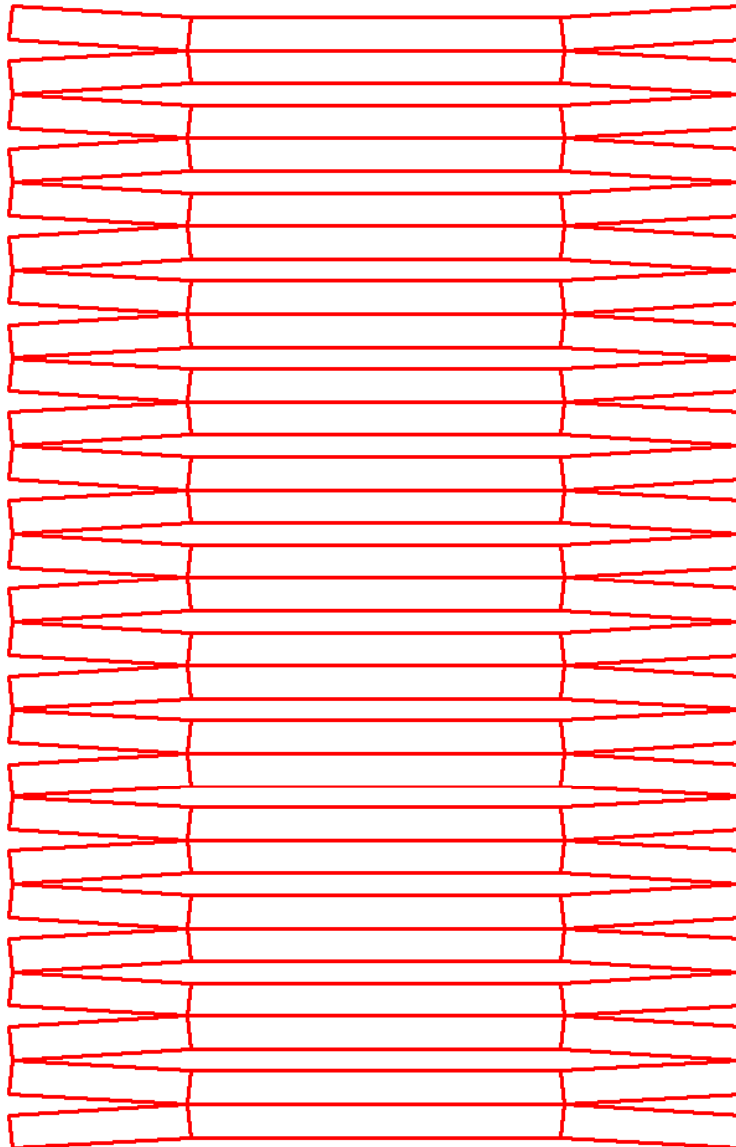
Ln = 100.8

Lc = 91

R1 = 16723 N/mm

R2 = 16723 N/mm

Complete Stack 26 springs



	A	B	C	D
1				
2		Calculations in (N and mm) units		
3				
4		Calcs Based on the SCHNORR data formulas.		
5				
6		Note: These calculations are for SCHNORR #15900 as basic shape		
7				
8				
9		De - Ouside diameter	60	mm
10		Di - Inside diameter	30.5	mm
11				
12		pi	3.14	
13		1/pi	0.3185	
14		3/pi	0.9554	
15		6/pi	1.9108	
16				
17		del=De/Di Schnorr Formula #2	1.9672	
18				
19		Indel=ln(De/Di)	0.6766	
20				
21		del-1	0.9672	
22		del+1	2.9672	
23				
24				
25				
26		(del-1/del)^2	0.2417	
27		(del+1)/(del-1)	3.0678	
28		(2/Indel)	2.9559	
29				
30				
31		K1=1/pi(((del-1/del)^2)/((del+1)/((del-1)-(2/Indel)))) Formula #3	0.6879	
32				
33		K2=6/pi(((del-1)/(Indel))-1))/((del+1)) Formula #4	1.2129	
34				
35		K3=3/pi(del-1/Indel) Formula #5	1.3657	
36				
37		K4=1 since thikness is less than 6 mm Formula #6 (see chapter	1	
38				
39				
40		FORCE and STRESS Calculations		
41				
42				
43				
44		lo= total height	5.004	mm
45		ho= lo-t	1.499	mm
46		t=average spring thickness	3.505	mm

Calculations based on SCHNORR catalogue equations for a single disk at constant compression
 $s = .364 \text{ mm}$

Stack compression in this case:
 $s = 9.47 \text{ mm.}$

Or $(.364 \times 26) = 9.47 \text{ mm.}$
 Force = 6,428. N
 ("HEXAGON" F=6,411 N)

See slide #2

47	s= deflection of the single spring (from 75% of ho))	0.364	mm
48	E= modulus for steel	206000	N/mm ²
49	mu= Poisson's ratio	0.3	
50	1-mu ²	0.91	
51	4E/(1-mu ²)	905494.505	
52	t ⁴ /(K1*de ²)	0.06094519	
53	s/t	0.10385164	
54	ho/t	0.42767475	
55	s/2t	0.05192582	
56			
57	Formula #8a	6428.45	N
58			
59	Formula #9 Stresses at the center of rotation (point OM)	-445.71	N/mm ²
60	(should be less then -1600N/mm ²)		
61	t ² /(K1*de ²)	0.00496093	
62			
63	formula #10 Stress at point (I)	-849.75	N/mm ²
64			
65			
66	formula #11 Stress at point (II)	424.527204	N/mm ²
67			
68			
69	formula #12 Stress at point (III)	459.19	N/mm ²
70			
71	1/del	0.50833333	
72	(K2-2K3)	-1.5185995	
73	(ho/t-s/2t)	0.37574893	
74			
75	Formula #13 Stress at point (IV)	-188.56	N/mm ²
76			
77	t ³ /(K1*de ²)	0.01738807	
78			
79	Formula #14 Spring Rate (dF/ds)	16781.43	N/mm
80			
81	Formula #15 Spring Work (Integral from 0 to s, of F*ds)	1190.33	N-mm
82			
83	2E/(1-mu ²)	452747.253	
84	t ⁵ /(K1*de ²)	0.2136129	
85			
86	Basic requirements for a good Disk spring design		
87	For the above basic equations to work		
88			
89	This Spring is linear because ho/t=.428 (since for ho/t<0.4 are li	slightly non-LINEAR	
90			
91	del=De/Di=2.3923 and it should be between 1.75 and 2.5	O.K.	
92	Outside diameter De, Inside diameter Di		

93			
94	$h_o/t = (l_o - t)/t = .428$ and it should be between 0.4 to 1.3	O.K.	
95	$h_o = l_o - t$ cone height, t =disk thickness		
96			
97	$D_e/t = 17.12$ and it should be between 16. and 40.	O.K.	
98			
99	Conclusion: This spring under the constant load of 3790.0 N is O.K.		
100			
101			
102	Basic machine operation requirements:		
103	1) TF coil inner leg maximum thermal expansion was calculated at 8.4mm		
104	2) OH coil requires a preload of 20,000.0 lbs total or 7,413.3 N (12 St) per stack. Must		
105	calculate the required deflection (s) for the preload force?		
106	3) OH coil thermal expansion was calculated at 6.0mm		
107			
108	So, the total each spring stack travel is = 8.4+6.0+calculated from minimum preload		
109			
110	For Fatigue predictions, using fatigue life diagrams for disk springs, one requires		
111	the Pre and Maximum loads stresses at points II or III (depending on $d_e l$ and h_o/t)		
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