

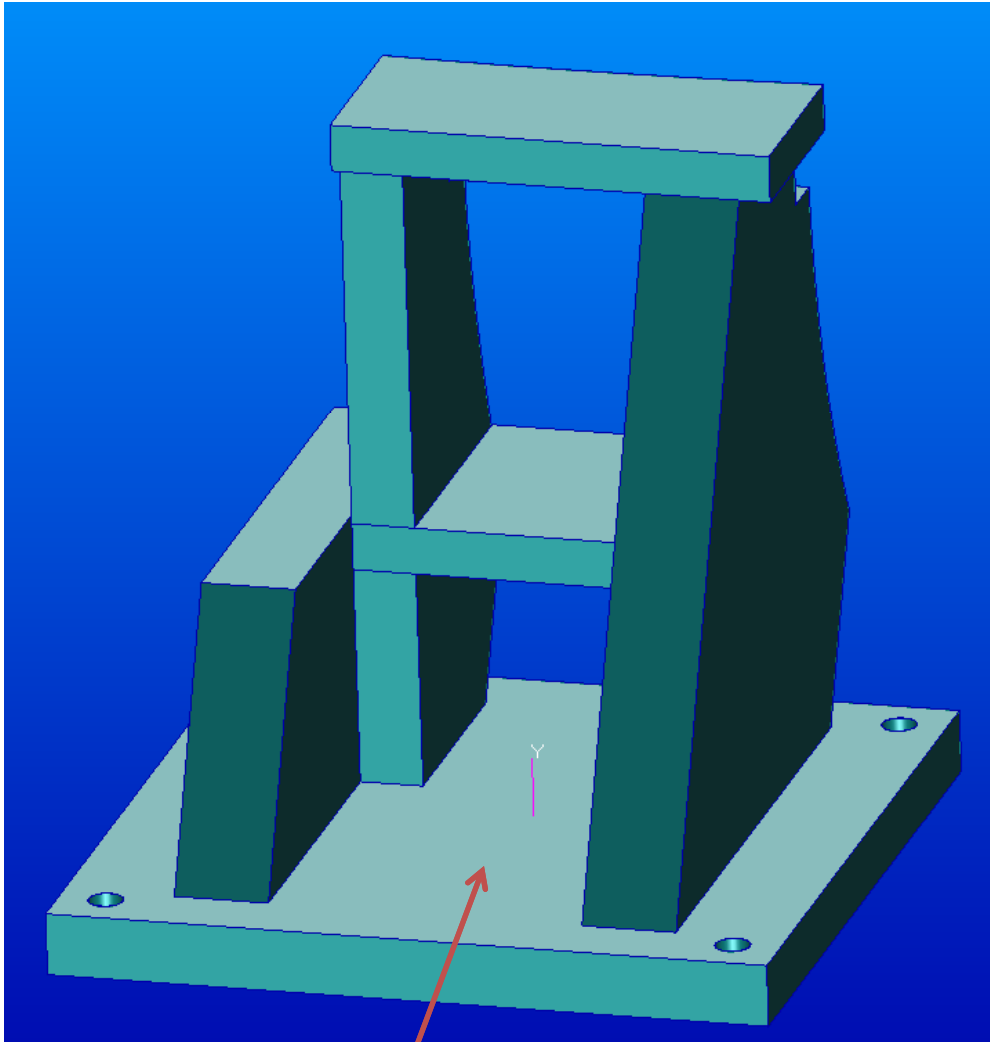
Vessel Support Leg Calculations

Enclosed are all the so far available calculations covering the above subject. Please note that this is preliminary presentation format and it may change as completion of the analyses progresses? I think, so far it is self explanatory.

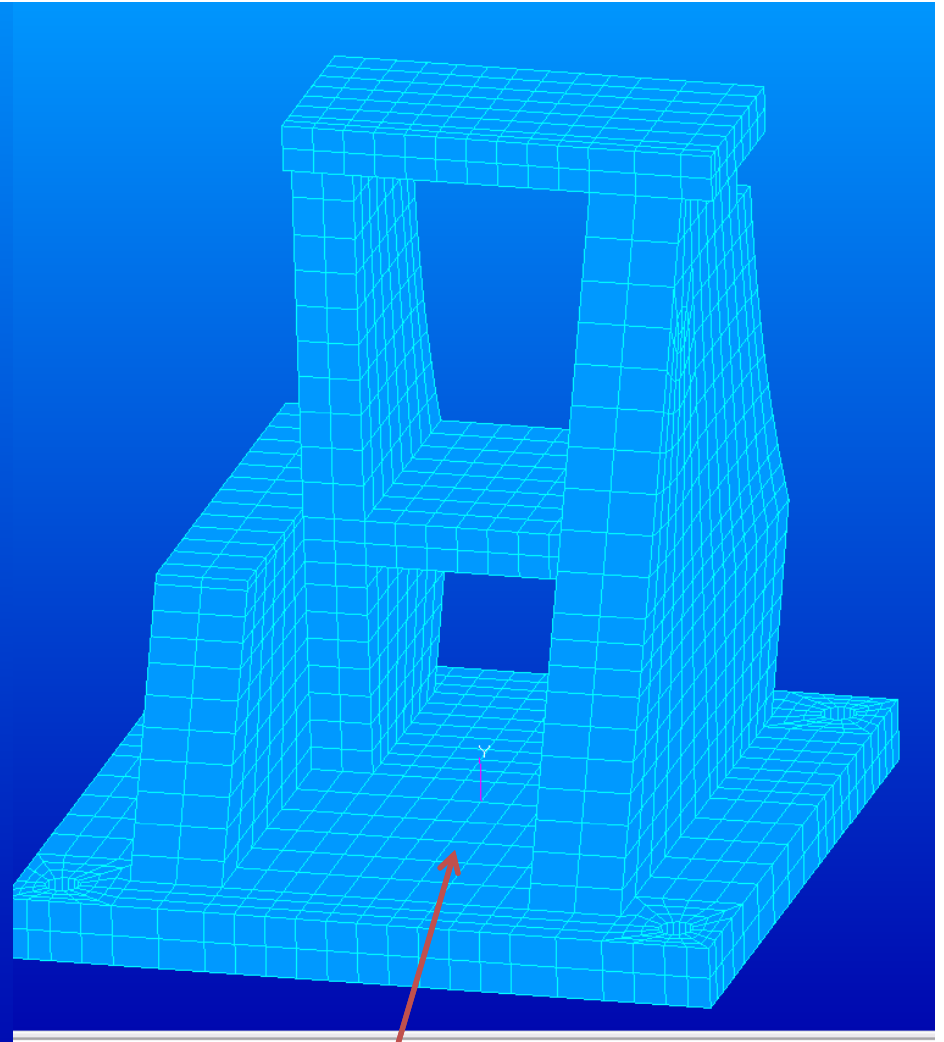
I am following a logical analyses progression from linear to non linear methods. I hope that this will answer all necessary questions.

Also, I have not fully completed RUN #4 analyses (Non Linear static Sol 106 with GAP elements). As you can see from the enclosed slides, many GAPs are involved. But, I think it will be done soon?

Please examine the included slides!



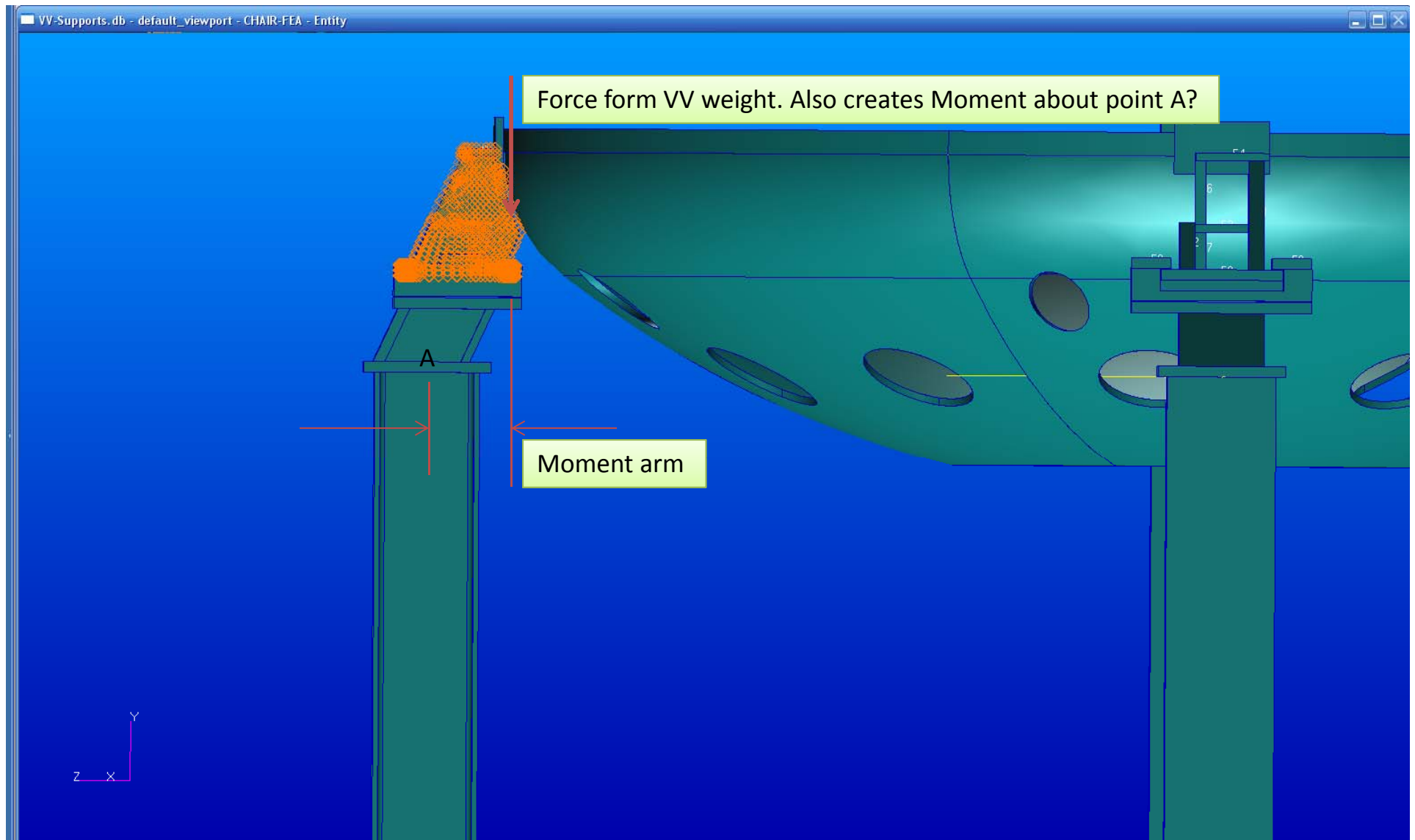
VV-support-attach-011812.igs



Nastran FEA all Hex8 elements

Question: How is this welded, assume weld size = $\frac{3}{8}$ inch?

Redesigned VV support chair



General design

VV Support configuration FEA simulation

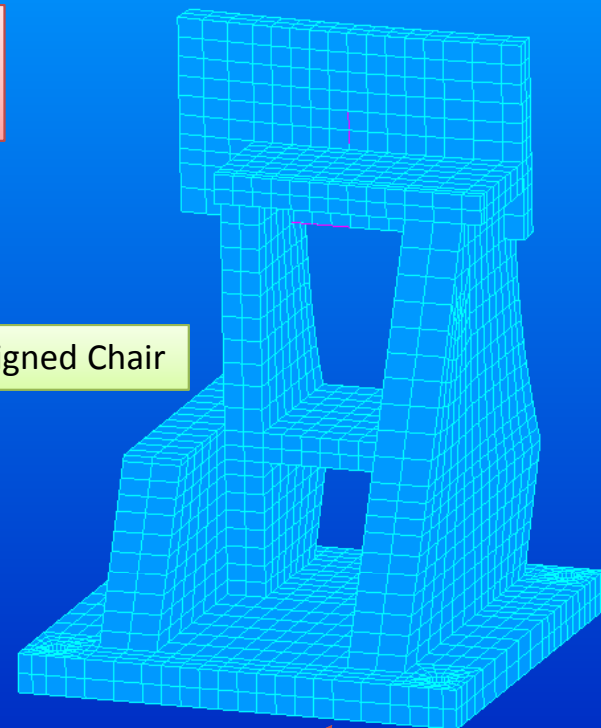
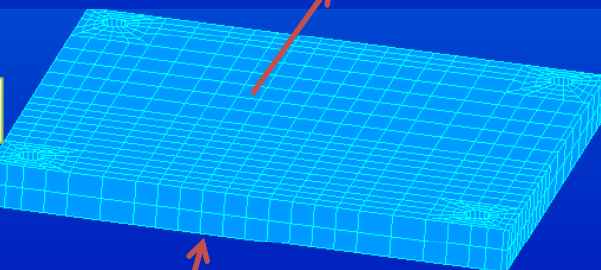
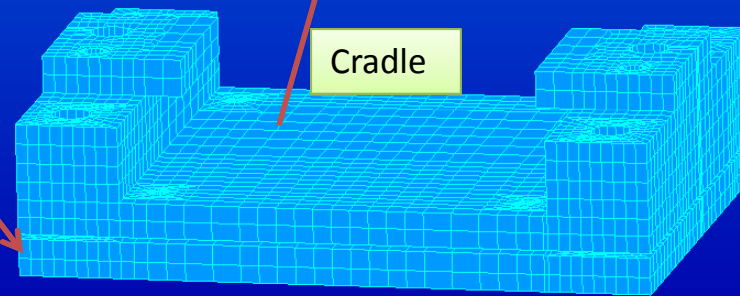
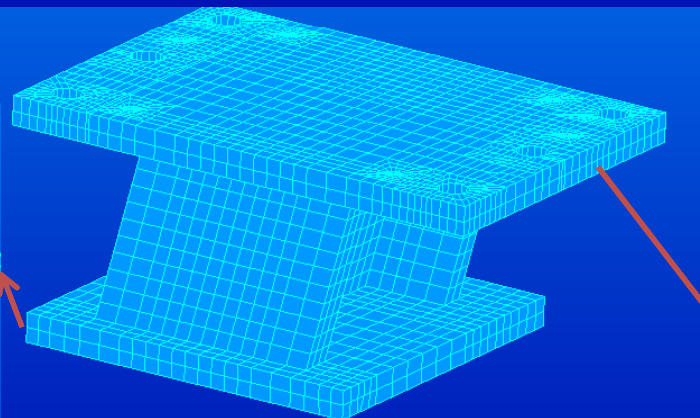
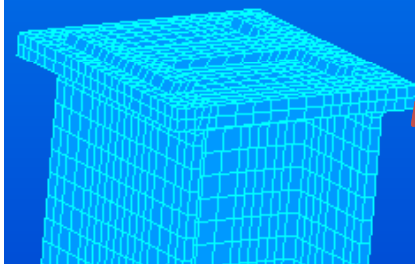
MPCs simulate
Cyclic Symmetry
3 – dof (1,2,3)
Hexa 8- elements

SPCs (1,2,3)
Fixity where
Braces are
located

Redesigned Chair

Slide plate

Cradle



RUN # 1

Static Test run #1 and Simulation general loads and fixities

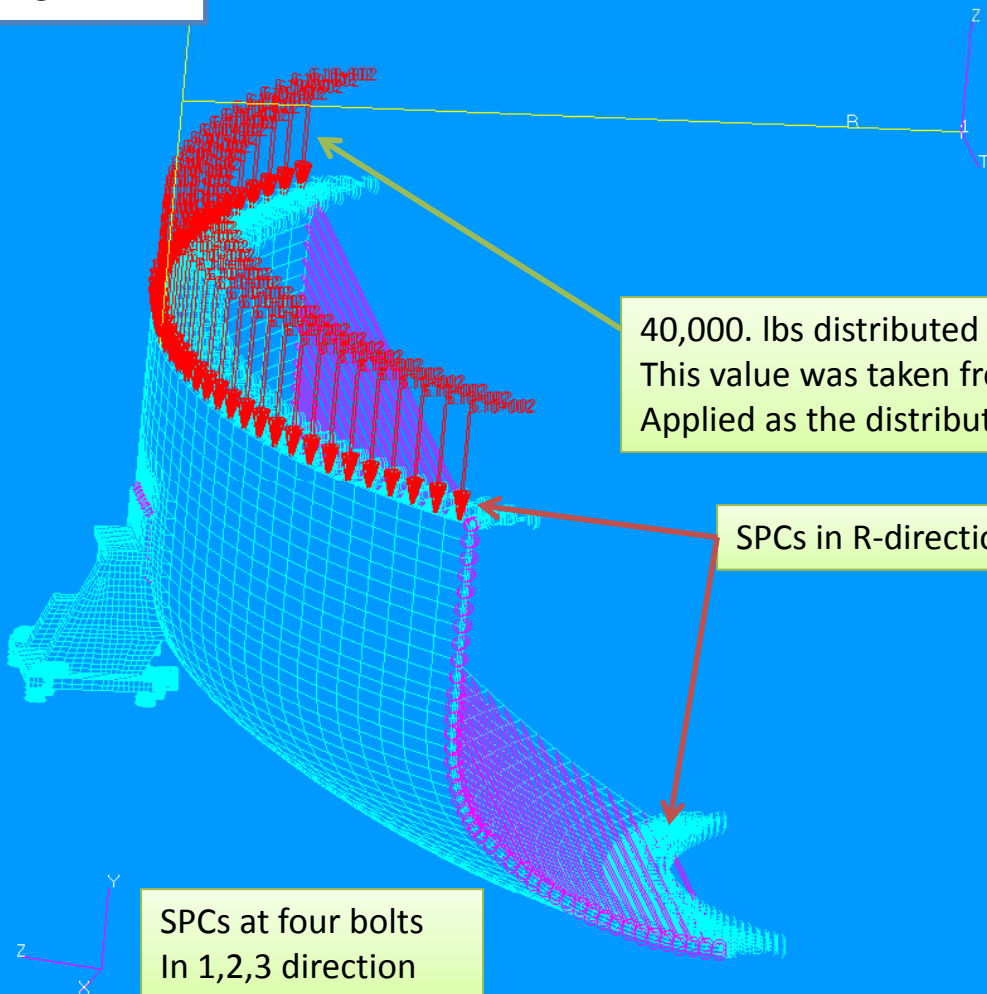
Db --- Statics
File -- ChairVVStatics.bdf
This is a test run to check
Connections to the VV

40,000. lbs distributed over the VV thickness and 45 degree sector.
This value was taken from the previous analyses estimates, It is
Applied as the distributed pressure.

SPCs in R-direction only

SPCs at four bolts
In 1,2,3 direction

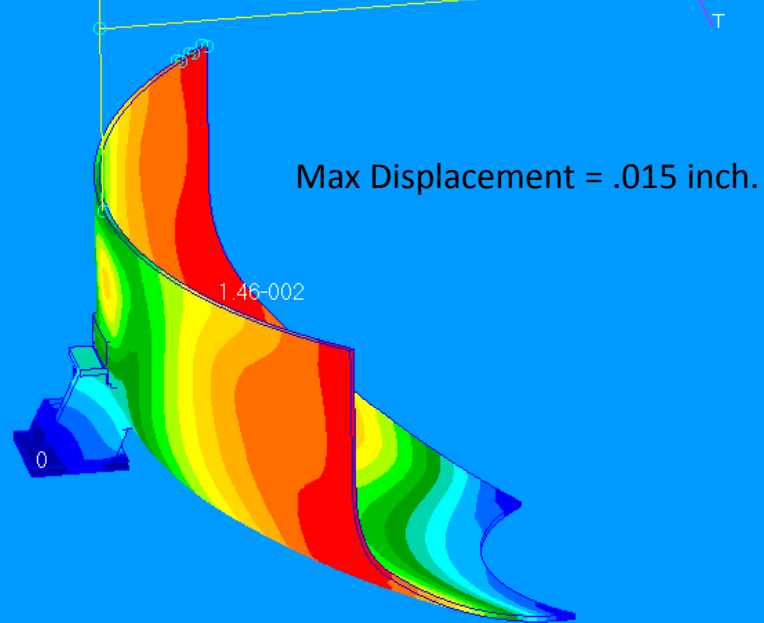
Results are in ChairVVStatics.xdb



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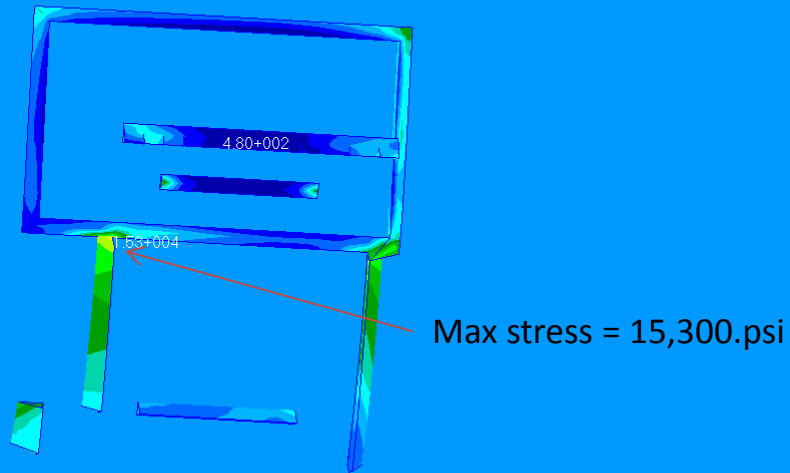
Fringe: Default, A1:Static Subcase, Displacements, Translational, Magnitude, (NON-LAYERED)

RUN # 1 Results



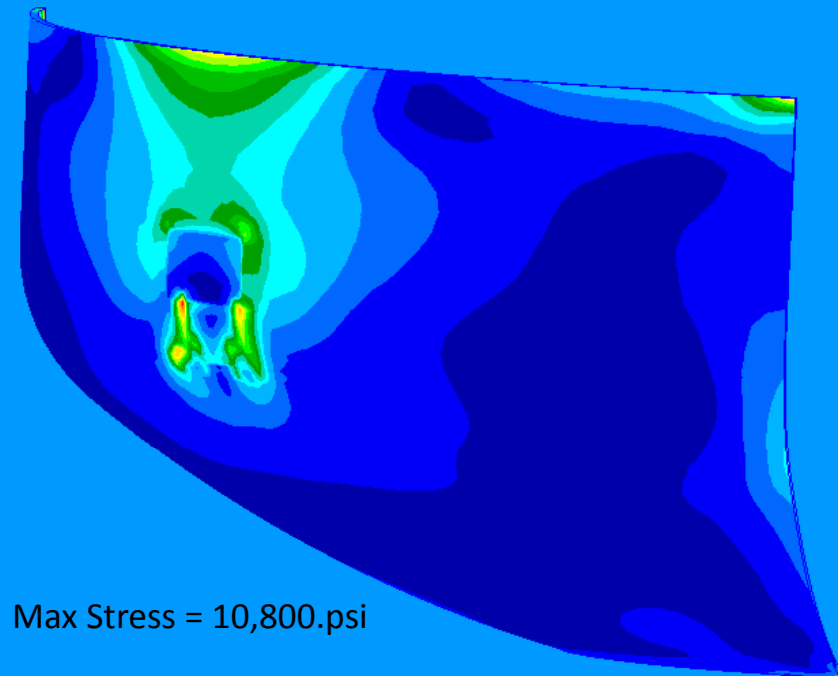
MSC FEA 2010.1.2 64-Bit 24-Feb-12 11:47:06

Fringe: Default, A1:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)



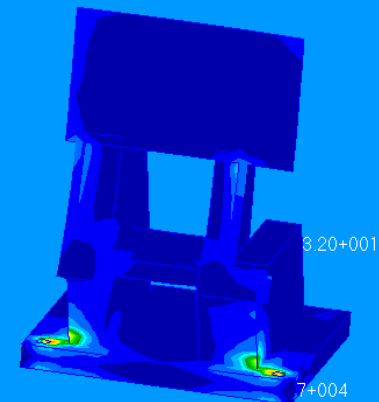
MSC FEA 2010.1.2 64-Bit 24-Feb-12 11:44:14

Fringe: Default, A1:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)



MSC FEA 2010.1.2 64-Bit 24-Feb-12 11:52:31

Fringe: Default, A1:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)



RUN #2

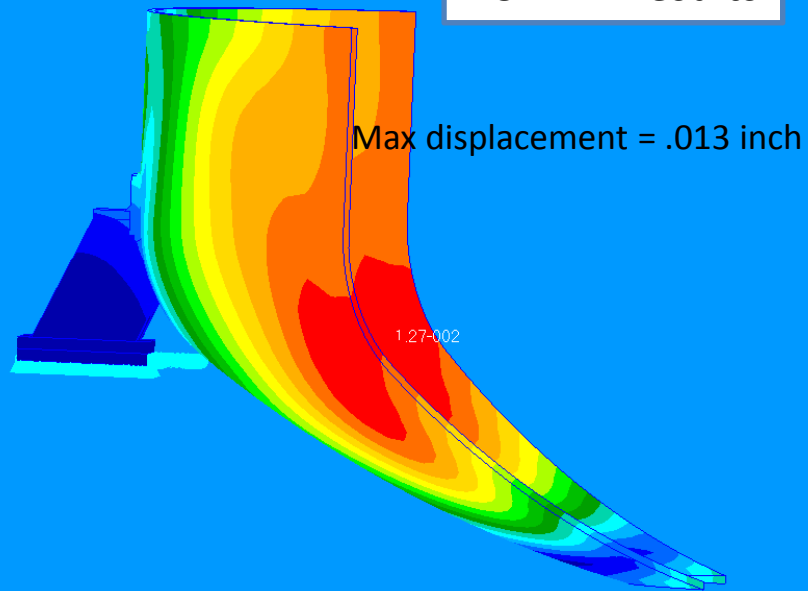


Added the slide plate and connected it via RBE2s to the chair with B.C. as shown. Sliding in the R- direction nodes at the center of the slide plate. (Y in coord1=0.)

MSC FEA 2010.1.2 64-Bit 28-Feb-12 13:46:02

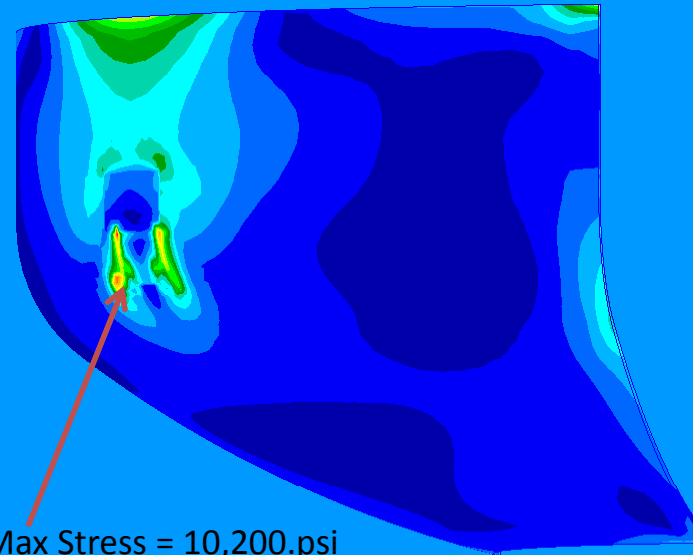
Fringe: RUN2-Loads, A2:Static Subcase, Displacements, Translational, Magnitude, (NON-LAYERED)

RUN #2 Results



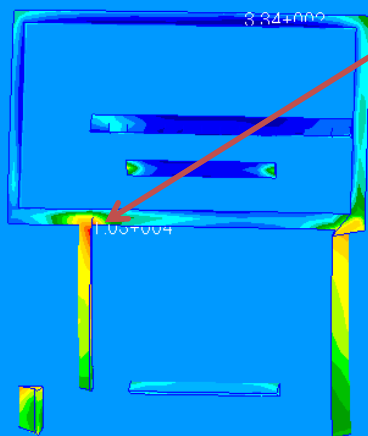
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Fringe: RUN2-Loads, A2:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)



MSC FEA 2010.1.2 64-Bit 28-Feb-12 14:10:36

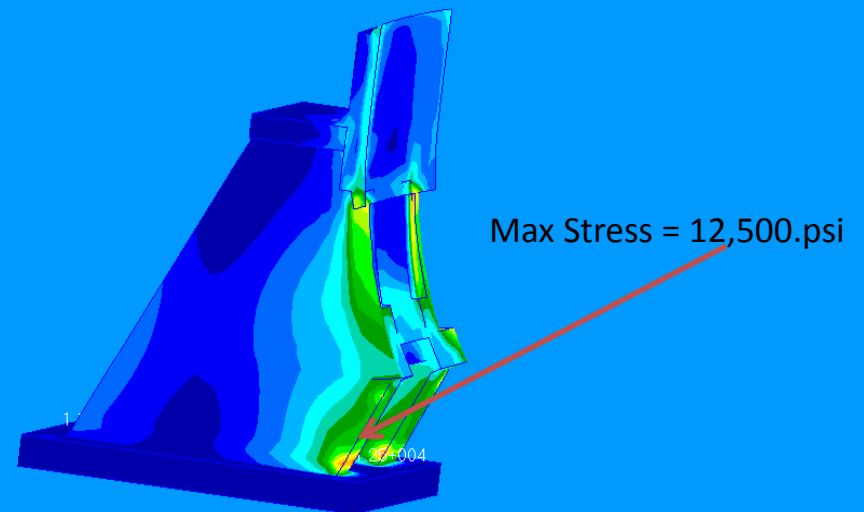
Fringe: RUN2-Loads, A2:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)



Welds between the Chair and the VV

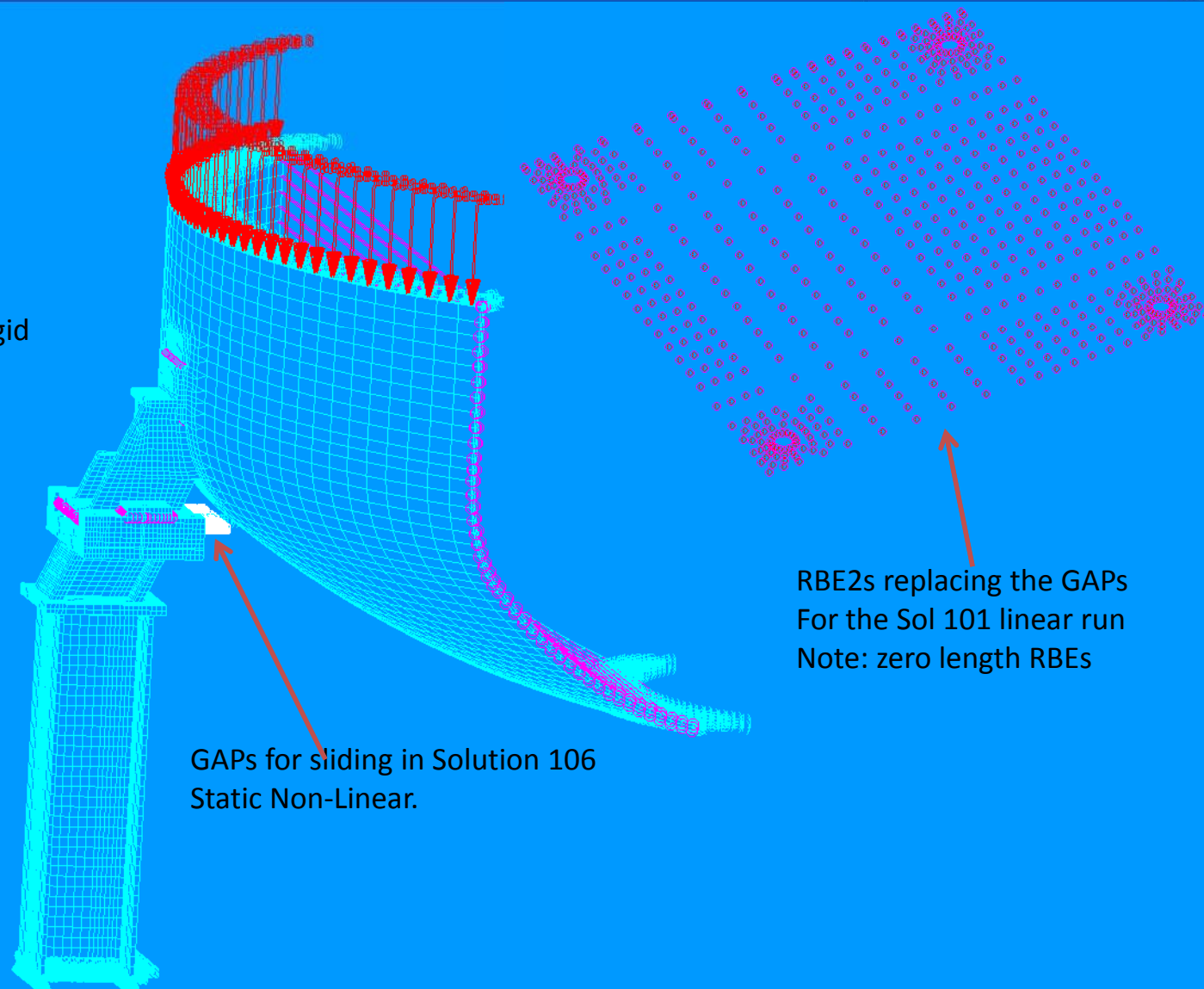
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Fringe: RUN2-Loads, A2:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)



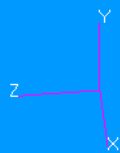
RUN #3

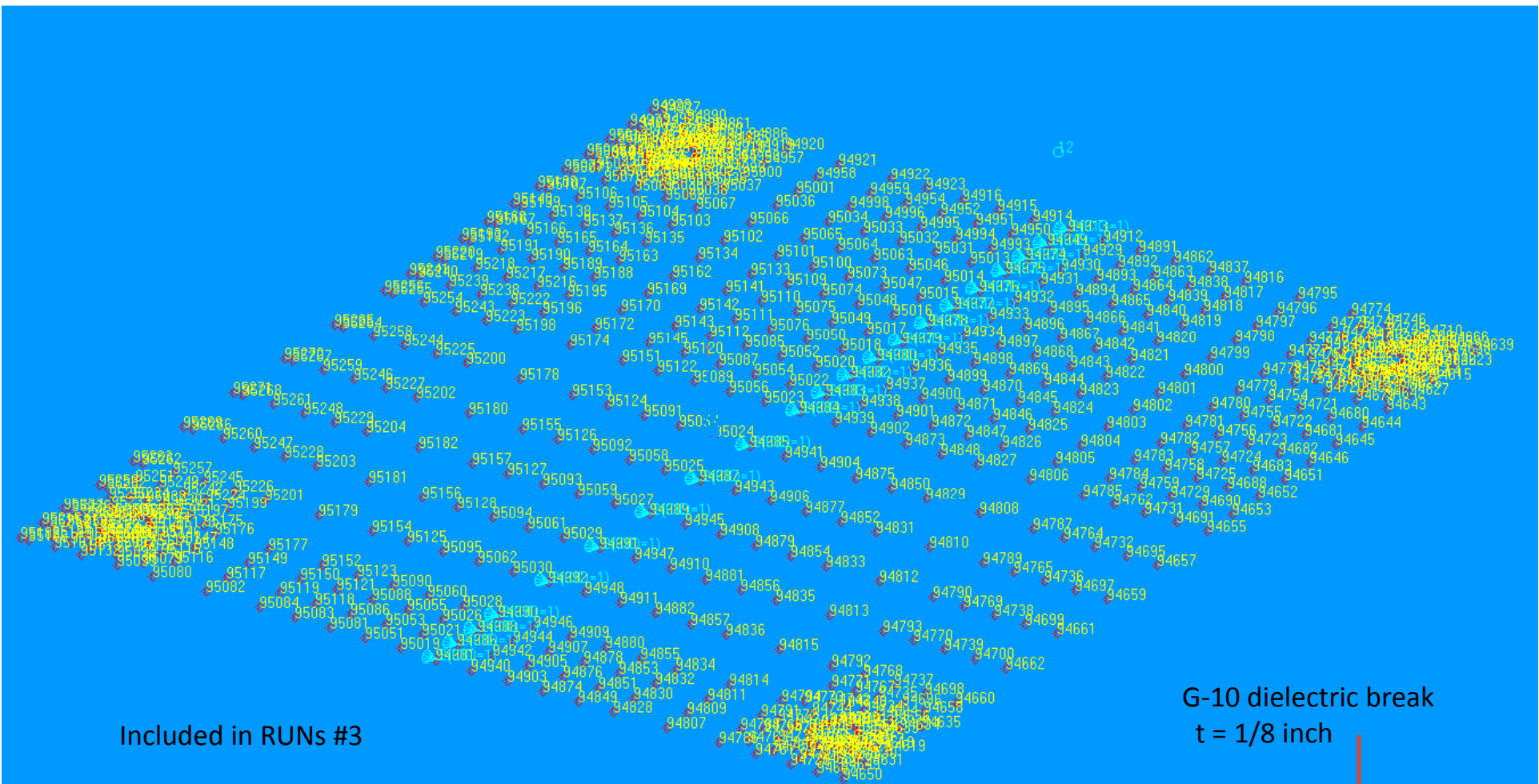
Sol 101 – Linear static run
With GAPS that become rigid
in this solution.



GAPs for sliding in Solution 106
Static Non-Linear.

RBE2s replacing the GAPs
For the Sol 101 linear run
Note: zero length RBEs

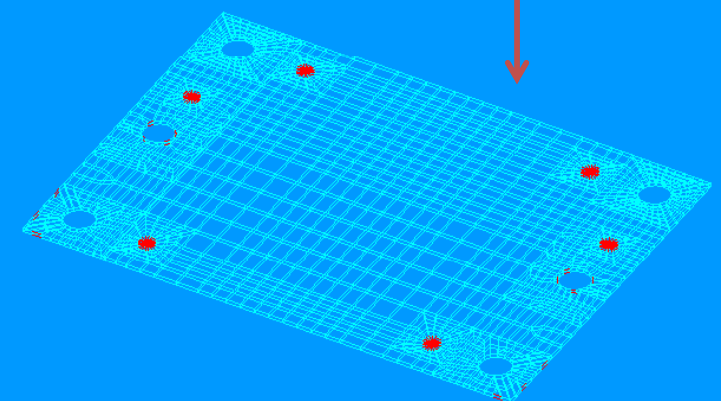




Included in RUNS #3

G-10 dielectric break
t = 1/8 inch

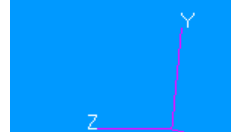
```
PARAM      POST      0
PARAM      PRTMAXIM YES
$ Elements and Element Properties for region : sliding-Gaps
PGAP       1         0.          3.+7      500.      1.+7      .3      .3
-1.
$ Pset: "sliding-Gaps" will be imported as: "pgap.1"
CGAP       94612     1          102192    127702    0.        -1.      0.
CGAP       94613     1          102195    128013    0.        -1.      0.
CGAP       94614     1          102199    128016    0.        -1.      0.
CGAP       94615     1          102201    128015    0.        -1.      0.
CGAP       94616     1          102204    131457    0.        -1.      0.
```



Between the cradle and Vertical support

Fringe: RUN3_Loads, A3:Static Subcase, Stress Tensor, , von Mises, (NON-LAYERED)

RUN #3 Results



Maximum stress on the total system for this run = 15,400. psi.

RUN #3 Results

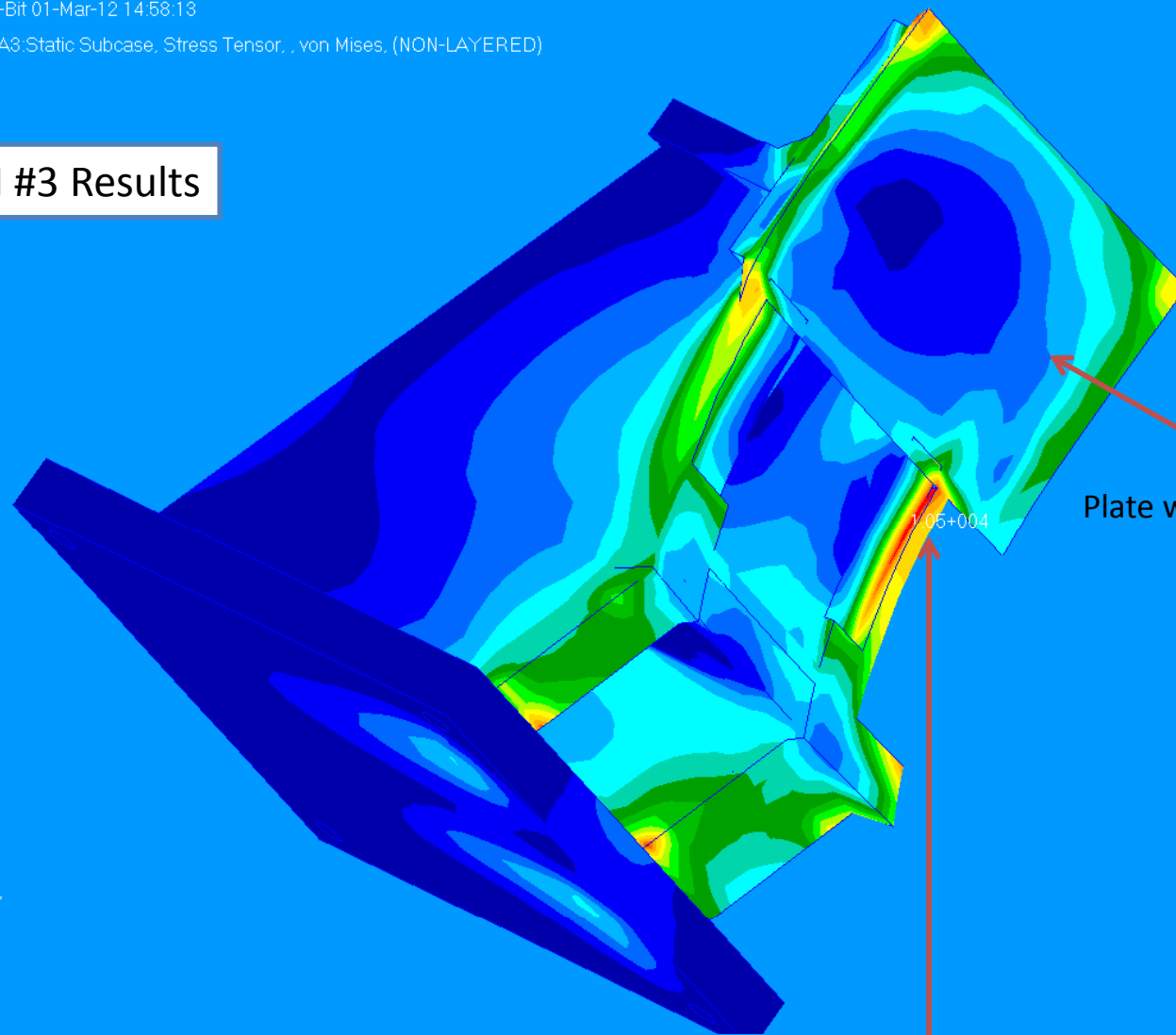


Plate welded to the VV

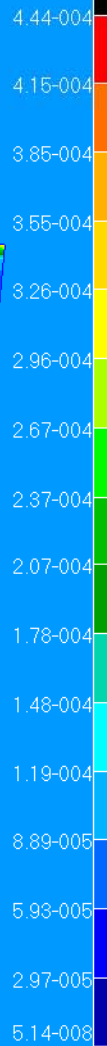
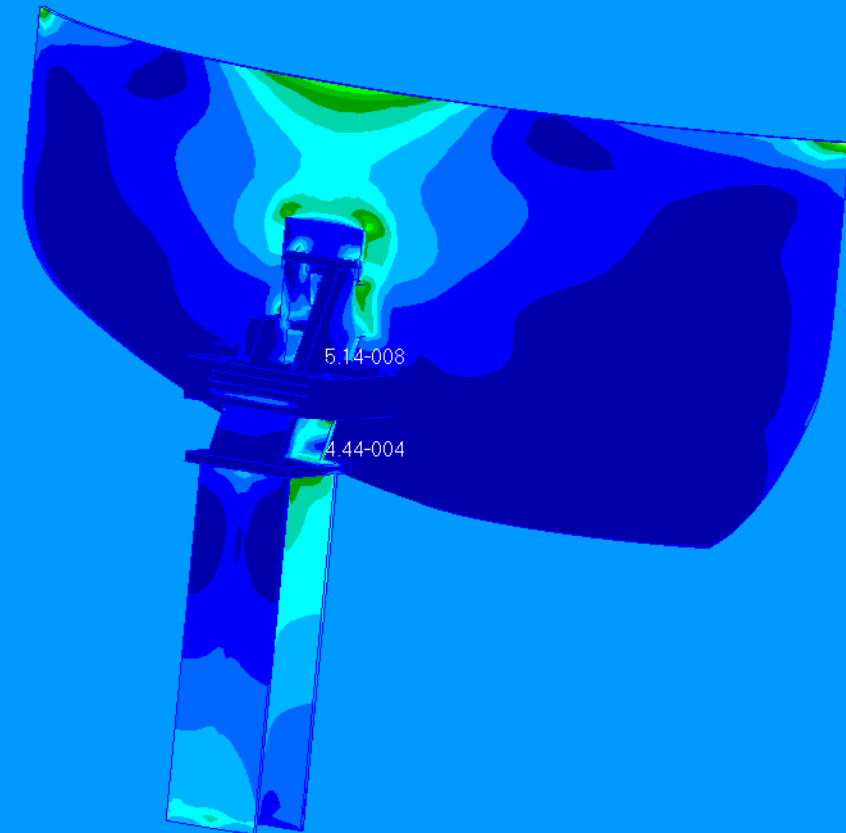
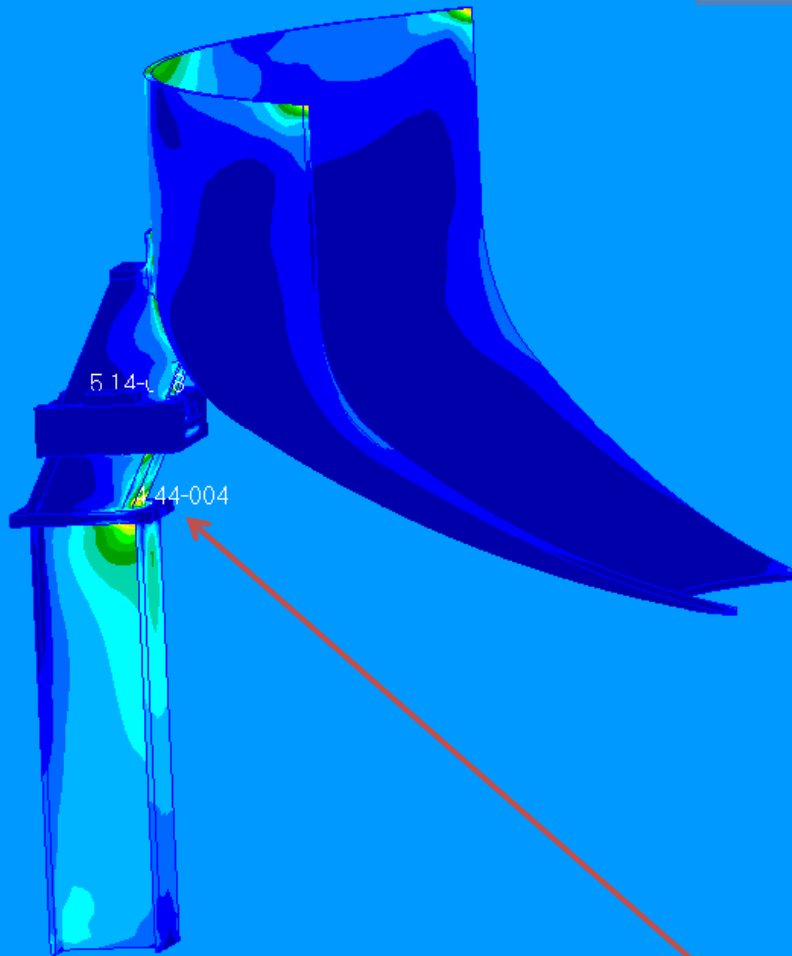
VV Chair with welds, Maximum Stress = 10,500.psi

1.05+004
9.77+003
9.08+003
8.38+003
7.68+003
6.98+003
6.29+003
5.59+003
4.89+003
4.20+003
3.50+003
2.80+003
2.11+003
1.41+003
7.13+002
1.57+001

default_Fringe :
Max 1.05+004 @Nd 13113

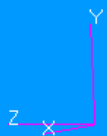
default_Fringe :
Max 1.05+004

RUN #3 Results



Maximum strain on the total system for this run = .00044

default_Fringe :
Max 4.44-004 @Nd 138632



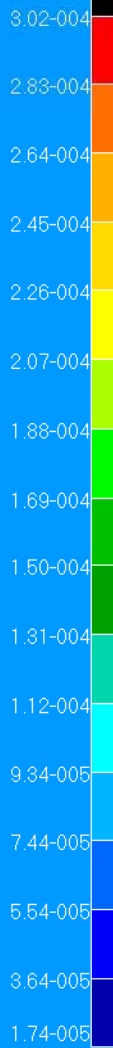
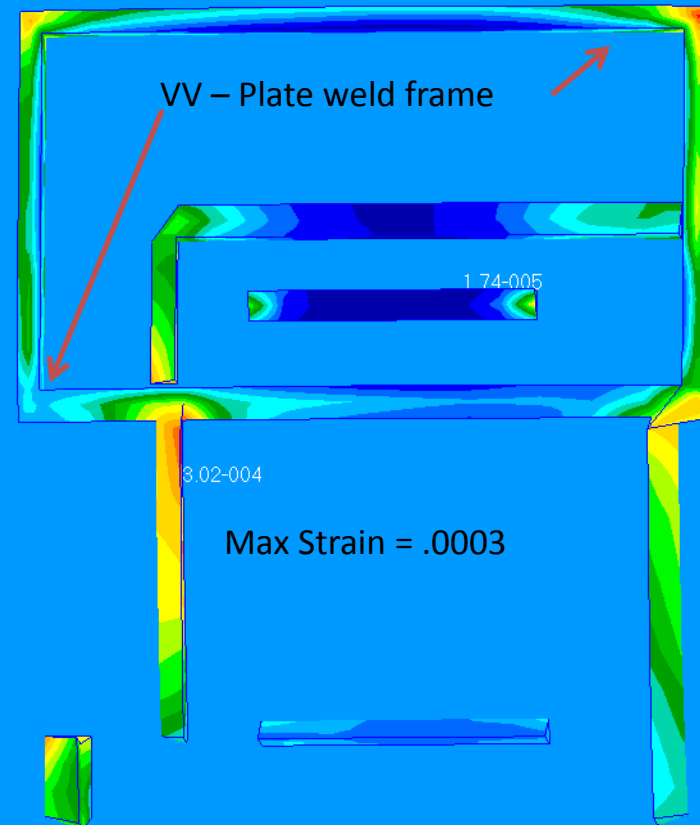
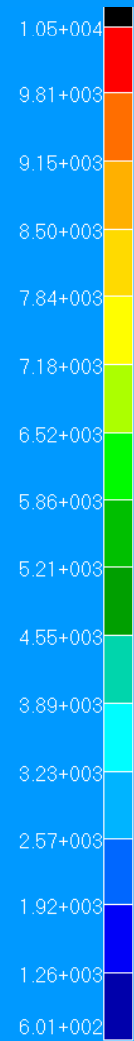
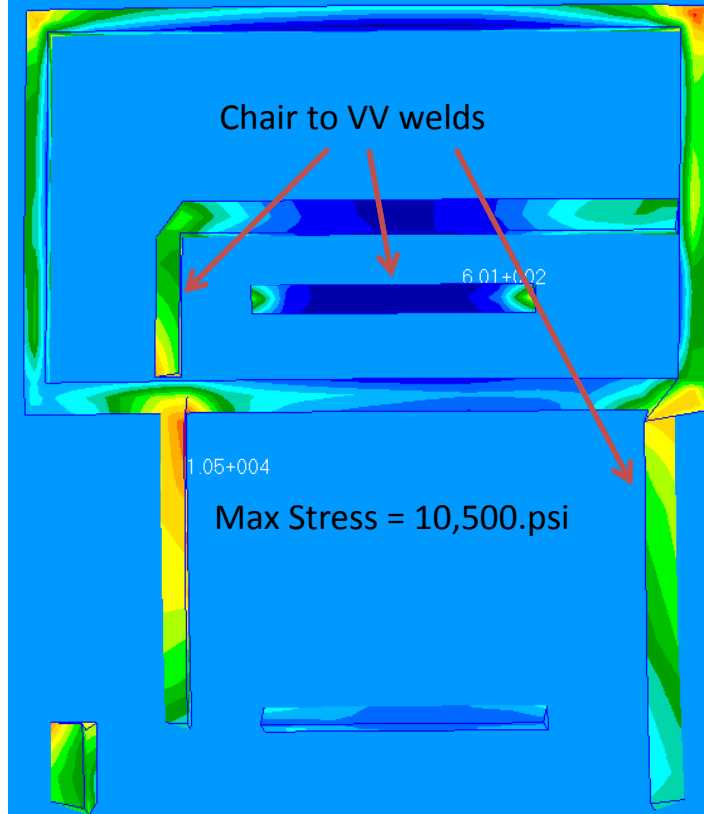
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Fringe: RUN3_Loads, A3:Static Subcase, Strain Tensor, ... (NON-LAYERED)

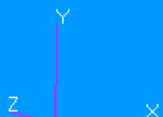
MSC FEA 2010.1.2 64-Bit 02-Mar-12 08:24:09

Fringe: RUN3_Loads, A3:Static Subcase, Stress Tensor, von Mises, (NON-LAYERED)

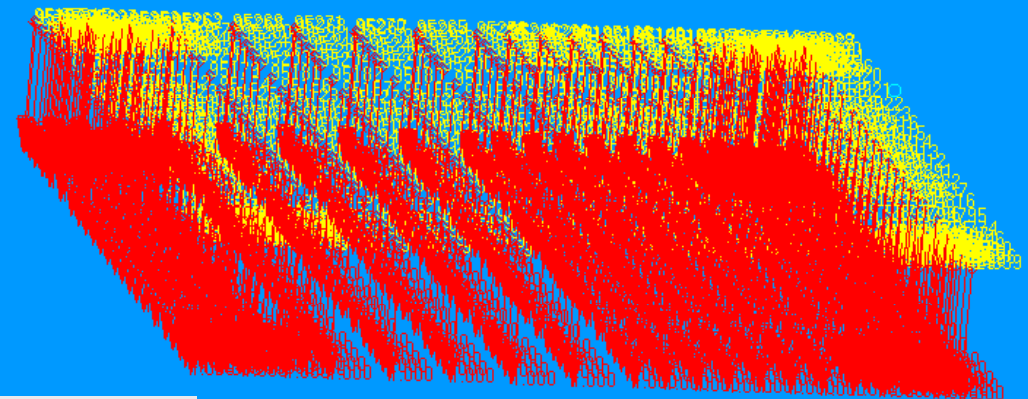
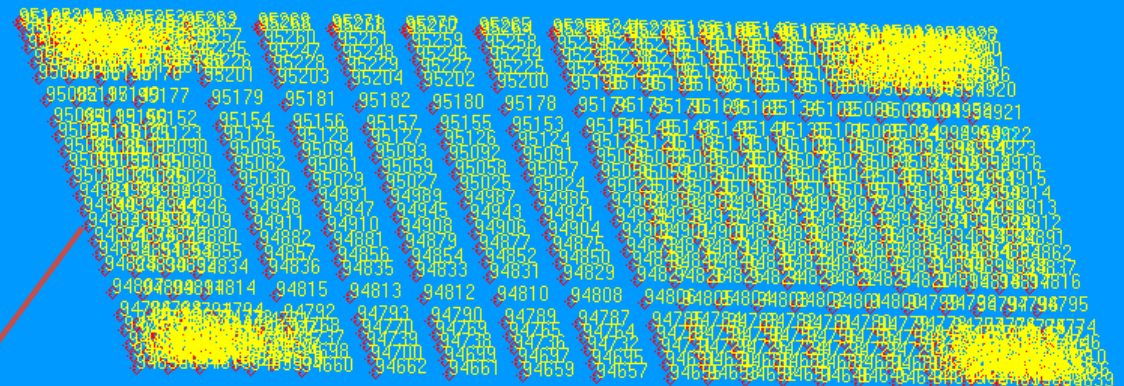
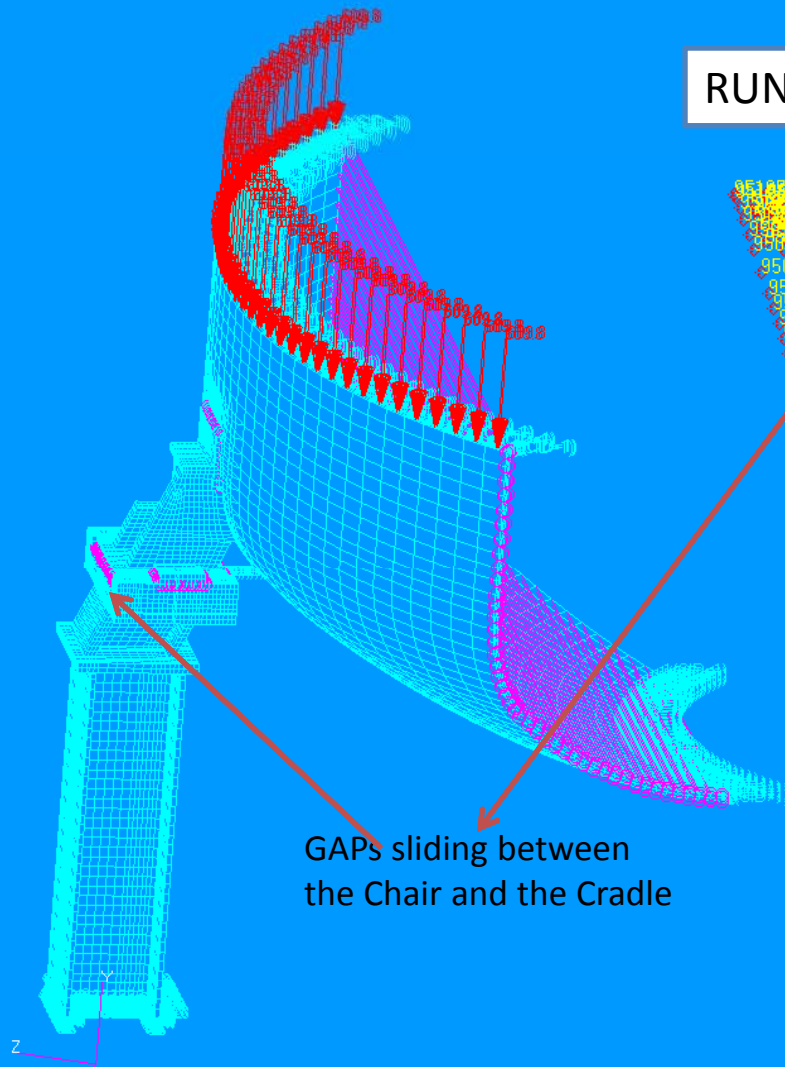
RUN #3 Results



default_Fringe :
Max 3.02-004 @Nd 13113
Min 1.74-005 @Nd 12001



RUN #4 Non Linear static Sol 106



	Type	Scale Factor	Priority
Slide_Fic_cen	Displacement	1.	Add
Support_Bot	Displacement	1.	Add
VV-Fixity	Displacement	1.	Add
VV-Fixity-Bot	Displacement	1.	Add
Pres40000	Pressure	1.	Add

Load Case "RUN4-Loads"

This is continuing with the non linear evaluation ?

P.R. 03/02/2012