TITLE__ Upgraded Center Stack Bakeout Ohmic Heating
CALC. NO.__ NSTXU-CALC-33-01-00_DATE__ 7/9/09


## PURPOSE:

This calculation determines the ohmic resistance of the NSTX CSU center stack casing, and the requirements for a power supply capable of supplying 5 kW of heat to same during bakeout.

During bakeout a current shall be injected at the bottom of the center stack casing (CSC) which shall flow up through the center stack casing, through four jumpers to the outer vacuum vessel (VV) upper dome, down through the VV dome to the cylinder, down through the VV cylinder, down through the lower VV dome, and out.

## REFERENCES:

1) INCONEL Alloy 625 data sheet (Huntington Metals)
2) NSTX Preliminary Dimension of CS Casing Drawing (attached)
3) NSTX-CALC-33-1 Center Stack Bakeout Ohmic Heating

## ASSUMPTIONS:

1) Neglect resistance of flanges which connect the center stack casing mid section to the end sections, and the flanges at the end sections. Compared to the resistance of the mid and end sections, the resistance of the flanges is not signficant due to their larger cross section and smaller length.
2) Treat the domes as flat disks. Assume that the current enters and exits the domes at the same ID as that of the CSC (in fact the current will not have to traverse the full length.
3) Neglect the effect of contact resistances, the holes/ports in the VV, etc.

## CALCULATION:

See attached spreadsheet entitled "CSU Ohmic Heating".
For the CSC, simple $\mathrm{R}=\rho \mathrm{l} / \mathrm{A}$ calculations are performed.

For the domes, treated as flat disks (like washers with inner radius R0 and outer radius R1), the effective resistance is calculated as follows:

Resistance of incremental section of the disk....

$$
\mathrm{R}=\rho \Delta \mathrm{r} / 2 \pi \mathrm{rt}
$$

Where:
$\mathrm{R} \quad=$ resistance of incremental disk section
$\rho \quad=$ resistivity
$\mathrm{r} \quad=$ radius
$\Delta r \quad=$ incremental radius
t = disk thickness
Total resistance...

$$
\begin{gathered}
\mathrm{Rt}=\int \rho \mathrm{dr} / 2 \pi \mathrm{rt} \\
=\rho \ln (\mathrm{r}) / 2 \pi \mathrm{t}
\end{gathered}
$$

Where:

Rt = total resistance of disk
The integral is evaluated between R0 and R1 such that:

$$
\mathrm{Rt}=\rho / 2 \pi \mathrm{t}^{*}(\ln (\mathrm{R} 1)-\ln (\mathrm{R} 0))
$$

The resistance at room temperature ( $\approx 20 \mathrm{C}$ ) is roughly $0.47 \mathrm{~m} \Omega$. The resistance at maximum bakeout temperature $(350 \mathrm{C}$ ) is roughly $0.48 \mathrm{~m} \Omega$. To produce 5 kW in the CS casing, an rms current of roughly 3.6 kA is required at bakeout temperature.

Note: all digital documents stored in NSTX File Share, Engineering Folder, Engineering Calculations Folder. Hard copies of all documents stored in NSTX project file.

## CONCLUSION:

Resistance of CS casing is such that ohmic heating using a small power supply is feasible. Resistance does not change very much over the temperature range. A rectifier power supply fed from a 480 V input, turned on/off via a thermostat type control, is suitable. The power supply should be rated to deliver on-state current equal to $1 / 0.0005 \approx 125 \mathrm{x}$ the voltage rating, due to the $0.5 \mathrm{~m} \Omega$ resistance (e.g. 3 V supply should be able to deliver 3.75 kA ). The rms rating should be at least 3.6kA.

CSU Ohmic Heating.xlsx

|  | A | B | C | D | E |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | INCONEL DATA SHEET... |  |  |  |  |
| 2 | T1 | 70.0 | deg F | 70.0 |  |
| 3 |  | 21.1 | deg C | $=5 / 9 *(B 2-32)$ |  |
| 4 | T2 | 800.0 | deg F |  |  |
| 5 |  | 426.7 | deg C | $=5 / 9 *(B 4-32)$ |  |
| 6 | Inconel Resistivity @ T1 | 776.0 | $\Omega$-circ mil/ft | 776.0 |  |
| 7 | Conversion factor | $1.97 \mathrm{E}+05$ | circ mil/sq cm | $1.97 \mathrm{E}+05$ |  |
| 8 | Conversion factor | 30.48 | $\mathrm{cm} / \mathrm{ft}$ | $=12 * 2.54$ |  |
| 9 | Inconel Resistivity @ T1 | 1.29E-04 | $\Omega-\mathrm{cm}$ | =B6/B7/B8 |  |
| 10 |  | $5.08 \mathrm{E}-05$ | $\Omega$-in | = $\mathrm{B} 9 / 2.54$ |  |
| 11 | Inconel Resistivity @ T2 | 818.0 | $\Omega$-circ mil/ft | 818.0 |  |
| 12 | Coefficient of resistance | 0.00013 | 1/deg C | $=(\mathrm{B} 11-\mathrm{B} 6) / \mathrm{B} 6 /(\mathrm{B} 5-\mathrm{B} 3)$ |  |
| 13 |  |  |  |  |  |
| 14 | Drawing NSTX EDC 1102/1107.. |  |  |  |  |
| 15 | ID Mid Section | 22.790 | in | 22.790 |  |
| 16 | Wall Mid Section | 0.188 | in | 0.188 |  |
| 17 | Length Mid Section | 89.050 | in | 89.050 |  |
| 18 | ID End Section | 30.000 | in | 30.000 |  |
| 19 | Wall End Section | 0.250 | in | 0.250 |  |
| 20 | Length End Flange | 3.500 | in | 3.500 |  |
| 21 | Length End Section (each) | 12.700 | in | =16.2-B20 |  |
| 22 |  |  |  |  |  |
| 23 | CS Resistance Calculations... |  |  |  |  |
| 24 | Radius Mid Section | 11.395 | in | - $\mathrm{B} 15 / 2$ |  |
| 25 | Thickness Mid Section | 0.188 | in | = B16 |  |
| 26 | Cross Section Mid Section | 13.571 | in^2 | $=\mathrm{Pl}() *((\mathrm{~B} 24+\mathrm{B} 25) \wedge 2-\mathrm{B} 24 \wedge 2)$ |  |
| 27 | Length Mid Section | 89.050 | in | = B17 |  |
| 28 | Resistance Mid Section (T1) | 3.33E-04 | $\Omega$ | =rest*B27/B26 |  |
| 29 | Radius End Sections | 15 | in | = B18/2 |  |
| 30 | Thickness End Sections | 0.250 | in | =B19 |  |
| 31 | Cross Section End Section | 23.758 | in 12 | $=\mathrm{Pl}()^{*}((\mathrm{~B} 29+\mathrm{B} 30) \wedge 2-\mathrm{B} 29 \wedge 2)$ |  |
| 32 | L End Section | 12.70000 | in | = B21 |  |
| 33 | Resistance per End Section (T1) | $2.71 \mathrm{E}-05$ | $\Omega$ | =rest*B32/B31 |  |
| 34 | $\Sigma$ Resistance Mid + 2 Ends (T1) | $3.87 \mathrm{E}-04$ | $\Omega$ | $=\mathrm{B} 28+2$ * 333 |  |
| 35 | Bakeout Temperature (T3) | 350.0 | C | 350.0 |  |
| 36 | $\Sigma$ Resistance Mid + 2 Ends (T3) | 4.04E-04 | $\Omega$ | $=\mathrm{B} 34 *\left(1+\mathrm{B} 12^{*}(\mathrm{~B} 35-\mathrm{B} 3)\right)$ |  |
| 37 |  |  |  |  |  |
| 38 | Return Path Through VV... |  |  |  |  |
| 39 | Resistivity 304SS | $7.7 \mathrm{E}-07$ | $\Omega-\mathrm{m}$ | 0.00000077 |  |
| 40 |  | $3.03 \mathrm{E}-05$ | $\Omega$-in | =B39*100/2.54 |  |
| 41 | VV Dome Wall | 0.625 |  | =5/8 |  |
| 42 | VV Cylinder Diameter | 134.25 | in | 134.25 |  |
| 43 | VV Cylinder Wall | 0.625 | in | $=5 / 8$ |  |
| 44 | VV Cylinder Height | 74 | in | 74 |  |
| 45 | RO Dome | 15 |  | = B 29 |  |
| 46 | R1 Dome | 67.125 |  | - B42/2 |  |
| 47 | Resistance per dome | $3.05 \mathrm{E}-05$ | $\Omega$ |  |  |
| 48 | VV Cylinder CSA | 131.4928 | in^2 | $=\mathrm{Pl}()^{*}((\mathrm{~B} 42 / 2) \wedge 2-((\mathrm{B} 42-\mathrm{B43}) / 2) \wedge 2)$ |  |
| 49 | VV Cylinder Resistance | $1.71 \mathrm{E}-05$ | $\Omega$ | =B40*B44/B48 |  |
| 50 |  |  |  |  |  |
| 51 | Sum Total Resistance (CS @ T1) | $4.66 \mathrm{E}-04$ | $\Omega$ | $=\mathrm{B} 34+2$ * $477+\mathrm{B} 49$ |  |
| 52 | Sum Total Resistance (CS @ T3) | $4.83 \mathrm{E}-04$ | $\Omega$ | = $\mathrm{B} 36+2$ * $477+$ B49 |  |
| 53 |  |  |  |  |  |
| 54 | Power Supply Calculations... |  |  |  |  |
| 55 | Power in CS Casing | 5000.000 | watt | 5000.000 |  |
| 56 | I for P @ T1 (note) | 3592.262 | amp | =SQRT(B55/B34) |  |
| 57 | $V$ for P @ T1 (note) | 1.672 | volt | = $556 *$ B51 |  |
| 58 | Total Power | 6007.852 | watt | $=\mathrm{B} 56 *$ B57 |  |
| 59 | I for P @ 33 (note) | 3515.930 | amp | =SQRT(B55/B36) |  |
| 60 | V for P @ T3(note) | 1.697 | volt | =B59*B52 |  |
| 61 | Total Power | 5965.475 | watt | = $\mathrm{B} 59 \times \mathrm{B60}$ |  |
| 62 |  |  |  |  |  |
| 63 |  |  |  |  |  |
| 64 |  |  |  |  |  |

